

BEFORE THE NEW MEXICO PUBLIC REGULATION COMMISSION

IN THE MATTER OF THE APPLICATION FOR)
THE LOCATION OF THE CLINES CORNERS)
WIND FARM AND GEN-TIE SYSTEM IN)
TORRANCE AND GUADALUPE COUNTIES)
PURSUANT TO THE PUBLIC UTILITY ACT, NMSA)
1978, §§62-9-3 AND 62-9-3.2)

Case No. 19 - _____

CLINES CORNERS WIND FARM, LLC)

APPLICANT.)

**DIRECT TESTIMONY
OF
GREG PARENT**

BEFORE THE NEW MEXICO PUBLIC REGULATION COMMISSION

IN THE MATTER OF THE APPLICATION FOR)
THE LOCATION OF THE CLINES CORNERS)
WIND FARM AND GEN-TIE SYSTEM IN)
TORRANCE AND GUADALUPE COUNTIES)
PURSUANT TO THE PUBLIC UTILITY ACT, NMSA)
1978, §§62-9-3 AND 62-9-3.2)
CLINES CORNERS WIND FARM LLC)
APPLICANT.)

Case No. 19 - 00139-JT

FILED IN OFFICE OF

MAY 15 2019

NM PUBLIC REGULATION COMM
RECORDS MGMT & INFORMATION DIVISION

DIRECT TESTIMONY OF

GREG PARENT

ON BEHALF OF CLINES CORNERS WIND FARM LLC

Case No. 19 - _____ - UT
Before the New Mexico Public Regulation Commission
Direct Testimony of Gregory Parent
on Behalf of Clines Corners Wind Farm LLC

1 **Q. PLEASE STATE YOUR NAME.**

2 A. Gregory Parent, P.E., S.E. The P.E. stands for licensed Professional Engineer and the S.E.
3 stands for licensed Structural Engineer.

4 **Q. BY WHOM AND IN WHAT CAPACITY ARE YOU EMPLOYED?**

5 A. I am employed by Ulteig Engineers, Inc. as a Senior Engineer in the Transmission and
6 Distribution Department. My business address is 5575 DTC Parkway, Suite 200,
7 Greenwood Village, CO 80111.

8 **Q. WHAT IS THE PURPOSE OF YOUR TESTIMONY IN THIS PROCEEDING?**

9 A. I am providing testimony on behalf of Clines Corners Wind Farm LLC (“Clines Corners”
10 or “Applicant”) which is a wholly owned subsidiary of Orion Wind Resources LLC
11 (“Orion Wind Resources”). Orion Wind Resources is owned by a joint venture between
12 Orion Renewable Energy Group LLC (“Orion”), and MAP Energy®. The purpose of my
13 testimony is to provide information regarding the requested approval of a 150-foot right-
14 of-way (“ROW”) located within a 1-mile-wide corridor (“Clines Corners Gen-Tie System
15 Corridor”) for the development and permitting of a 18.72 mile 345-kilovolt (“kV”)
16 alternating current lines transmission system and associated transmission facilities (“Clines
17 Corners Gen-Tie System” or “Gen-Tie System”). The Clines Corners Gen-Tie System will
18 connect a wind generation facility of up to approximately 600 megawatts (“MW”) (“Clines
19 Corners Wind Farm”) to the proposed Western Spirit transmission line (“Western Spirit”)
20 at a point that is approximately 11 miles west-northwest of Encino (34.689855, -
21 105.647307). Collectively, the Clines Corners Wind Farm and the Gen-Tie System will be
22 referred to herein as the “Clines Corners Wind Farm Project” or “Project”.

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1 I will also provide information about the interconnection facilities where the Gen-Tie
2 System will connect the Clines Corners Wind Farm to Western Spirit.

3 **Q. PLEASE DESCRIBE YOUR EDUCATIONAL AND WORK EXPERIENCE.**

4 A. I have a Master of Science in Structural Engineering from Lehigh University. I am a
5 licensed P.E. in 18 states and am also a licensed Structural Engineer in Illinois, Hawaii,
6 Nevada and Utah. I am a New Mexico Professional Engineer and my license number is
7 24890. I have 10 years of transmission line design experience and have designed
8 approximately 675 miles of transmission line.

9 **Q. HAVE YOU PREVIOUSLY SUBMITTED TESTIMONY IN ANY OTHER PROCEEDING?**

10 A. Yes. In July 2018, I provided direct testimony before the Commission to support the
11 application of Ancho Wind LLC, Cowboy Mesa LLC, Duran Mesa LLC, Red Cloud Wind
12 LLC, Tecolote Wind LLC and Viento Loco LLC for location control approval of the
13 Corona Wind Projects under development by Pattern Energy Group 2 LP in Guadalupe,
14 Lincoln and Torrance Counties and its 345-kV transmission system and associated
15 facilities, including a 180-foot ROW located within a 1 mile-wide corridor. My
16 supplemental testimony was in support of the proposed ROW width for the Corona Gen-
17 Tie System.

18 **Q. ARE YOU FAMILIAR WITH THE PROPOSED PROJECT AND SPECIFICALLY THE PROPOSED**
19 **GEN-TIE SYSTEM?**

20 A. Yes. I have worked closely with Orion personnel, including Michael Kurnik and Ryan
21 McGraw, in the preliminary design of transmission facilities for this Project. More

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specifically, the ROW width requirement calculation for the Clines Corners Gen-Tie System was performed by Ulteig Engineers, Inc.

Q. WHAT ROW WIDTH WAS DETERMINED TO BE NEEDED FOR THE CLINES CORNERS GEN-TIE SYSTEM ACCORDING TO YOUR CALCULATIONS?

A. A 150-foot ROW width was determined to be necessary for the Gen-Tie System to connect the Clines Corners Wind Farm to Western Spirit and the electric transmission grid, in a safe and reliable manner. The 150-foot ROW width is necessary to provide sufficient space for variation in design, while addressing electrical safety code requirements and construction and operation considerations according to prudent and standard industry practice.

Q. CAN YOU ELABORATE ON THE BASIC DESIGN CONDITIONS YOU EVALUATED IN DETERMINING THAT A 150-FOOT ROW WAS REQUIRED FOR THIS PROJECT?

A. Yes. Preliminary design considerations include geotechnical soil studies, topographical surveys, conductor analysis and wind and weather patterns to determine a range of preliminary specifications for equipment and infrastructure for the proposed location for transmission and interconnection facilities. The loading conditions for the transmission lines meet or exceed the requirements stated in the National Electric Safety Code (NESC-2017). We analyzed the required ROW width for the following load cases:

1. NESC 234.C.1.a (At Rest)

a. 0 psf wind pressure acting perpendicular to the conductor

b. 60 deg Fahrenheit ambient temperature.

2. NESC 234.C.1.b (6 psf Wind)

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1 a. 6 psf wind pressure acting perpendicular to the conductor

2 b. 60 deg Fahrenheit ambient temperature

3 3. NESC 250B –Loading District. According to the NESC 250B Loading District Map
4 the district where the Clines Corners Gen-Tie System, transmission line, is located is
5 in the NESC 250B “Medium” loading district. However, Clines Corners has requested
6 that this transmission line be designed to resist the loads from the NESC 250B “Heavy”
7 loading district. Below are the loading conditions for the NESC 250B “Heavy” loading
8 district.

9 a. 4 psf wind pressure acting perpendicular to the conductor

10 b. ½” of radial ice

11 c. 0 deg Fahrenheit ambient temperature

12 4. NESC 250C – Extreme Wind. The wind load map in NESC 250C matches the basic
13 wind speed map in the American Society of Civil Engineers – Minimum Design Loads
14 for Building and Other Structures - ASCE 7-05. The Clines Corners Wind Farm
15 extends over a large region. The extreme wind speed varies over this region. Part of
16 the Clines Corners Wind Farm is in the 90-mph wind speed region but also extends
17 into a “Special Wind Region”. Special wind regions experience higher wind speeds
18 than 90 mph. Orion has determined that the extreme wind speed for these special wind
19 regions should be set at 100 mph. For consistency, the extreme wind speed for the
20 entire project has been set to 100 mph whether it is inside or outside the special wind
21 regions.

22 a. 100 mph wind speed (25.6psf) acting perpendicular to the conductor

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1 b. 60 deg Fahrenheit ambient temperature

2 Under these conditions, and the aforementioned considerations, I evaluated the clearances,
3 conductor movement, and structure deflection to calculate span lengths and structure types
4 and configurations.

5 **Q. DO YOU BELIEVE THAT THE CRITERIA YOU RELIED UPON IN DETERMINING THE**
6 **NECESSITY FOR A 150-FOOT ROW TO BE REASONABLE?**

7 A. Yes. These criteria are appropriate and consistent with the accepted practice within the
8 industry. I have designed approximately fifteen 345-kV transmission lines and the right of
9 way widths for those projects ranged between 150ft – 200ft. The variations in right of way
10 width for these projects depended on design spans, number of circuits supported by the
11 structure, structure types, conductor type and conductor tension, audible noise
12 requirements that were used on each line, and the aforementioned considerations.

13 **Q. DO YOU HAVE EXHIBITS SUPPORTING YOUR CALCULATIONS THAT WARRANT THE 150-**
14 **FOOT ROW WIDTH THAT THE APPLICANT REQUESTS IN THIS PROCEEDING?**

15 A. Yes. Please see the attached exhibit titled Exhibit GP-1.

16 **Q. PLEASE EXPLAIN THE INFORMATION CONTAINED IN EXHIBIT GP-1.**

17 A. Page 1 of this exhibit provides the calculations for the NESC required horizontal clearances
18 from the transmission line conductor to building structures for NESC Rules 234B1a,
19 234B1b. Also provided is the recommended horizontal clearance when the transmission
20 line is subject to 100 mph wind speed. The above clearances have been adjusted for an
21 elevation of 6,650 ft. The following pages of this Exhibit GP-1 illustrate the results of the
22 blowout analysis for a single circuit steel monopole tangent structure type.

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1 To determine conductor blowouts and pole deflections, the structure was modeled using a
2 bundled (2) 1272kcmil ASCR “Bittern” conductor per phase. To calculate the conductor
3 blowout, a 1,300 ft design span between structures was modeled. Actual design spans
4 could vary depending on the topography. A design span of 1,300 ft would be a maximum
5 design span. Pole heights were determined to provide adequate vertical clearance under
6 the conductor during maximum operating temperatures at mid-span assuming flat terrain.
7 Pole heights will vary due to the natural topography and the varying span length between
8 structures, but typical structures will be between 95ft and 120ft above grade.

9 Each structure type was analyzed under the following four different load cases:

- 10 1. NESC Rule 234B1a – [At Rest Condition, 0 psf wind, 60 degF]
- 11 2. NESC Rule 234B1b – [6psf Condition, 6 psf wind, 60 degF]
- 12 3. NESC Rule 250B – Heavy Region [4psf wind, ½” Radial Ice, 0 degF]
- 13 4. NESC Rule 250C – Extreme Wind [100 mph (25.6 psf), 60 degF]

14 To determine the conductor blowouts and pole deflections, each structure type and each
15 load case was modeled in the transmission line design software PLS-CADD. The results
16 of the required right of way width for each of the above load cases are illustrated in Exhibit
17 GP-1. The controlling load case was under NESC Rule 250C – Extreme Wind [100 mph
18 (25.6 psf), 60 degF]. This structure type and load case would require a minimum right of
19 way width approximately 131’-11” wide, which is less than requested 150’-0” ROW width.
20 A detailed analysis of the steel monopole structure under the 250C – Extreme Wind case
21 is provided on pages 5 and 6 of Exhibit GP-1.

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1 Page 7 of Exhibit GP-1 illustrates the “footprint” of a guyed heavy angle monopole
2 structure. A guyed heavy angle monopole structure uses guywires to resist the lateral loads
3 that are applied to the structure from the tensioned conductors. The guywires extend down
4 at an angle from the pole structure to the ground. Each guywire connects to a ground
5 anchor. For the guywires to remain within the 150ft ROW the pole structure would need
6 to be offset approximately 25 ft towards the inside edge of the ROW. Offsetting of the
7 structures from the centerline is not unusual within the transmission line industry. Page 7
8 of Exhibit GP-1 shows a 150ft ROW is wide enough to fit a guyed heavy angle monopole.
9 Page 8 of Exhibit GP-1 calculates the required ROW for the span between the 25 ft offset
10 guyed heavy angle monopole structure and the adjacent tangent structure under load case
11 NESC Rule 250C – Extreme Wind [100 mph (25.6 psf), 60 degF]. The blowout of the
12 conductor is largest at the midspan and therefore the blowout analysis was performed at
13 midspan. Since the guyed heavy angle monopole structure is offset 25ft from the
14 centerline, at the midspan between the adjacent tangent structure the conductors are offset
15 12ft 6in towards the inside edge of the ROW. The results show that even with this offset
16 the requested 150ft ROW is adequate, but the spans between the guyed heavy angle
17 monopole structure and the tangent structures should not exceed 1200ft.

18 Another calculation that was performed was the audible noise volume that would be heard
19 at the edge of the right of way. In 1974, the Environmental Protection Agency (“EPA”)
20 published *Information on Levels of Environmental Noise Requisite to Protect Public*
21 *Health and Welfare with an Adequate Margin of Safety* in which the EPA set 55dBA as the
22 outdoor noise threshold that would prevent activity interference or annoyance. Many

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1 utilities I have worked with have a 50dBA noise threshold limit at the edge of the right of
2 way.

3 Audible noise calculations were completed for the following structure types:

- 4 • Typical Tangent Monopole Structure (Page 9 of GP-1)
- 5 • Guyed Heavy Angle Monopole Structure (Page 10 of GP-1)

6 Page 9 of Exhibit GP-1 shows the calculations of the audible noise for the typical Steel
7 Tangent Monopole Structure. In this analysis the audible noise produced by the
8 transmission line, at midspan between two tangents, would be 49.9 dBA 75ft from the
9 transmission line center line ($75\text{ft} \times 2 = 150\text{ft}$ ROW). When the typical tangent is centered
10 in a right of way having a width of 150ft, the audible noise produced at the edge of the
11 ROW is just under the recommended 50dBA limit.

12 Page 10 of Exhibit GP-1 shows the calculations of the audible noise for the Guyed Heavy
13 Angle Steel Monopole Structure. As illustrated on page 7 of GP-1, the steel pole is offset
14 25ft toward the inside edge of the ROW. This locates the conductors only 50ft from the
15 inside edge of the ROW. In this analysis the audible noise produced by the conductors of
16 the Guyed Heavy Angle Steel Monopole Structure would be 49.97 dBA 75ft from the
17 transmission line center line ($75\text{ft} \times 2 = 150\text{ft}$ ROW). When the Guyed Heavy Angle Steel
18 Monopole Structure is offset 25ft from the centerline of a 150ft ROW, the audible noise
19 produced at the edge of the ROW is just under the recommended 50dBA limit.

20 **Q. BASED UPON YOUR ANALYSIS WHAT IS YOUR CONCLUSION WITH RESPECT TO THE**
21 **PROPOSED ROW WIDTH IN THE APPLICATION?**

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1 A. From the analysis I performed to determine required ROW widths, it is my professional
2 opinion that a right of way of 150ft is adequate for this line.

3 **Q. HOW WILL THE GEN-TIE SYSTEM INTERCONNECT THE CLINES CORNERS WIND FARM**
4 **TO WESTERN SPIRIT?**

5 Page 1 of exhibit GP-2 displays an Interconnection Map. This map is intended to illustrate
6 the different electrical systems used to connect the proposed Clines Corners Wind Farm to
7 the proposed Western Spirit transmission line. The electrical systems are made up of the
8 following three components:

9 1. The Clines Corners 34.5kV/345kV Collection Substation

10 (Please refer to CCW-SUB-EQ1 & CCS-SUB-OL1 drawings within exhibit
11 GP-2)

12 2. The Clines Corners 345kV 18.7-mile-long Transmission Line

13 (Please refer to GP-1)

14 3. The Western Spirit 345kV Switchyard / Point of Interconnect

15 (Please refer to CCW-INT-EQ1 & CCS-INT-OL1 drawings within exhibit GP-
16 2)

17 The Clines Corners 34.5kV/345kV collection substation contains numerous 34.5kV
18 feeders, and a 34.5kV/345kV transformer along with circuit breakers and switches. This
19 collection substation collects the power from the wind turbines and boosts the voltage from
20 34.5kV to 345kV so that the power can be transmitted over large distances without
21 experiencing large amounts of electrical loss. The Clines Corners 34.5kV/345kV
22 collection substation connects to the Clines Corners 345kV transmission line which carries

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1 the power a distance of approximately 18.7 miles within a ROW width of 150ft. The Clines
2 Corners 345kV transmission line then connects to a Western Spirit 345kV switchyard /
3 point of interconnect ("POI"). This POI is a three-breaker ring bus that consists of 3 bays,
4 3 breakers, 6 switches, and 9 metering units. The three-breaker ring bus can electrically
5 isolate any one of the three lines that connect to the switchyard. This three-breaker ring
6 bus will be the electrical system that connects the Clines Corners 345kV transmission line
7 to the Western Spirit 345kV line.

8 **Q. HAVE YOU DISCUSSED YOUR ANALYSIS WITH THE COMMISSION STAFF?**

9 A. Yes. I have provided copies of my analysis to the Commission staff and had the opportunity
10 to obtain their feedback and suggestions which I believe that I have addressed in this
11 testimony.

12 **Q. DOES THIS CONCLUDE YOUR TESTIMONY?**

13 A. Yes.

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1978, §§62-9-3 AND 62-9-3.2)
CLINES CORNERS WIND FARM, LLC)
APPLICANT.)

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EXHIBIT GP-1

Ulteig Engineering
 Project Name: Clines Corners Wind Farm Project
 Required NESC Horizontal Clearances - Rule 234B1a & 234B1b
 Engineer: Greg Parent
 Date: 03-25-19



(VN) = Nominal Operating Voltage Phase-Phase (kV) $V_N := 345 \text{ kV}$

(VM) = Max Transient Overvoltage Phase-Phase (kV) $V_M := 1.05 \cdot V_N = 362.25 \text{ kV}$

(Elev) = Design Elevation (ft) $Elev := 6650 \text{ ft}$

(CHAR) = Required Horizontal Clearance At Rest (ft) NESC RULE 234B1a

(CH@6psf) = Required Horizontal Clearance under 6psf (ft) NESC RULE 234B1b

(CH@100mph) = Recommended Horizontal Clearance under 100mph

$$CH_{AR} := 7.5 \text{ ft} + ((50 \text{ kV} - 22 \text{ kV})) \cdot \left(\frac{0.4 \frac{\text{in}}{\text{kV}}}{12 \frac{\text{in}}{\text{ft}}} \right) + \left(\frac{V_M}{\sqrt{3}} - 50 \text{ kV} \right) \cdot \left(\frac{0.4 \frac{\text{in}}{\text{kV}}}{12 \frac{\text{in}}{\text{ft}}} \right) \cdot 1.03 \frac{Elev - 3300 \text{ ft}}{1000 \text{ ft}}$$

$$CH_{AR} = 14.29 \text{ ft}$$

$$CH_{@6psf} := 4.5 \text{ ft} + ((50 \text{ kV} - 22 \text{ kV})) \cdot \left(\frac{0.4 \frac{\text{in}}{\text{kV}}}{12 \frac{\text{in}}{\text{ft}}} \right) + \left(\frac{V_M}{\sqrt{3}} - 50 \text{ kV} \right) \cdot \left(\frac{0.4 \frac{\text{in}}{\text{kV}}}{12 \frac{\text{in}}{\text{ft}}} \right) \cdot 1.03 \frac{Elev - 3300 \text{ ft}}{1000 \text{ ft}}$$

$$CH_{@6psf} = 11.29 \text{ ft}$$

$$CH_{@100mph} := 345 \text{ kV} \cdot \frac{0.1 \frac{\text{in}}{\text{kV}}}{12 \frac{\text{in}}{\text{ft}}} \cdot 1.03 \frac{Elev - 3300 \text{ ft}}{1000 \text{ ft}}$$

$$CH_{@100mph} = 3.174 \text{ ft}$$

Assuming 10kV per inch dielectric constant for air

CLINES CORNER
 WIND FARM
 TORRANCE COUNTY,
 NEW MEXICO

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A	03/02/19	PERMIT SUPPORT	UD
B	05/03/19	REVISED	UEI
C	05/07/19	REVISED	UEI

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 OAKLAND, CA 94612

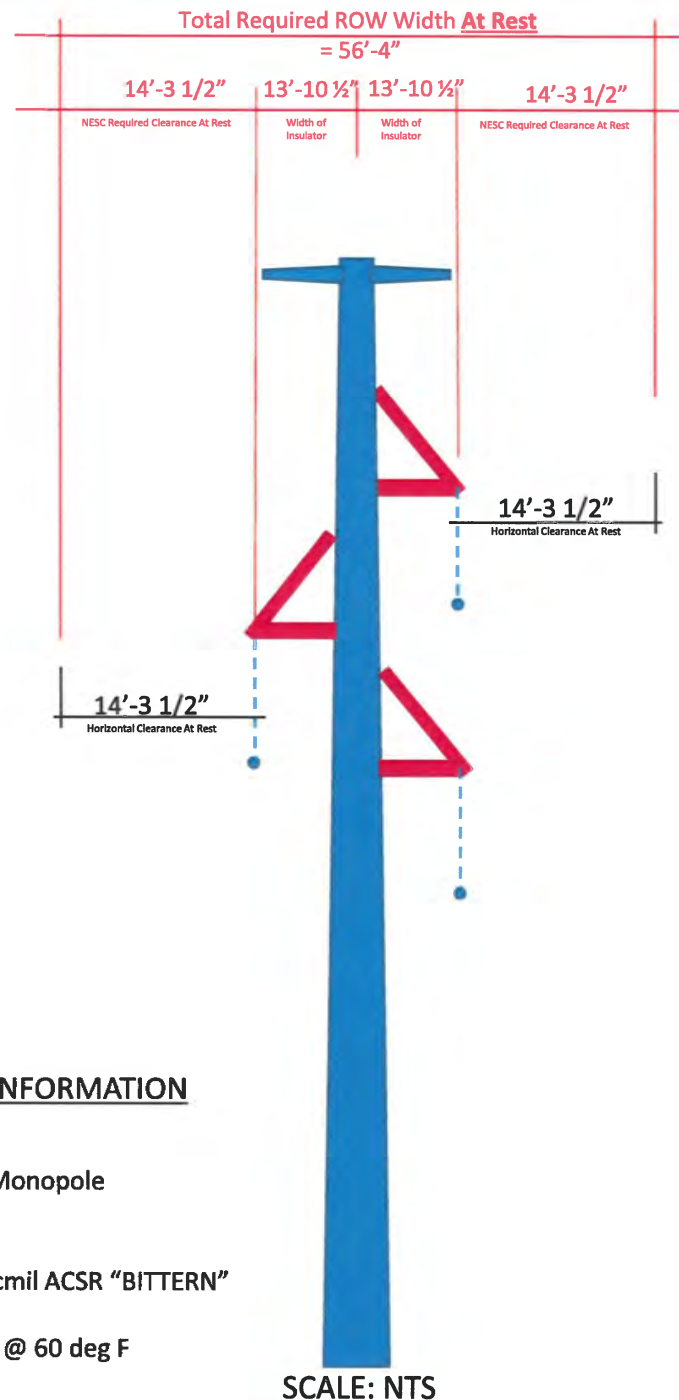


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 www.ulteig.com
 New Mexico Registration:
 Design By: G. PARENT
 Drawn By: B. CAMPBELL
 Approved By: G. PARENT
 Project Number:

NESC HORIZONTAL
 CLEARANCES UNDER
 BLOWOUT

DWG #: CCW-TRN-ROW-001
 REVISION C

Exhibit GP-1



STRUCTURE AND CONDUCTOR INFORMATION

Operational Voltage: 345kV
 Structure Type = Single Circuit Steel Monopole
 Insulator Type = Brace-Post Insulator
 Maximum Design Span = 1300ft
 Conductor Type = Bundled (2) 1272kcmil ACSR "BITTERN"
 NESC Rule Analyzed: 234B1a
 Weather Condition Displayed = 0 PSF @ 60 deg F

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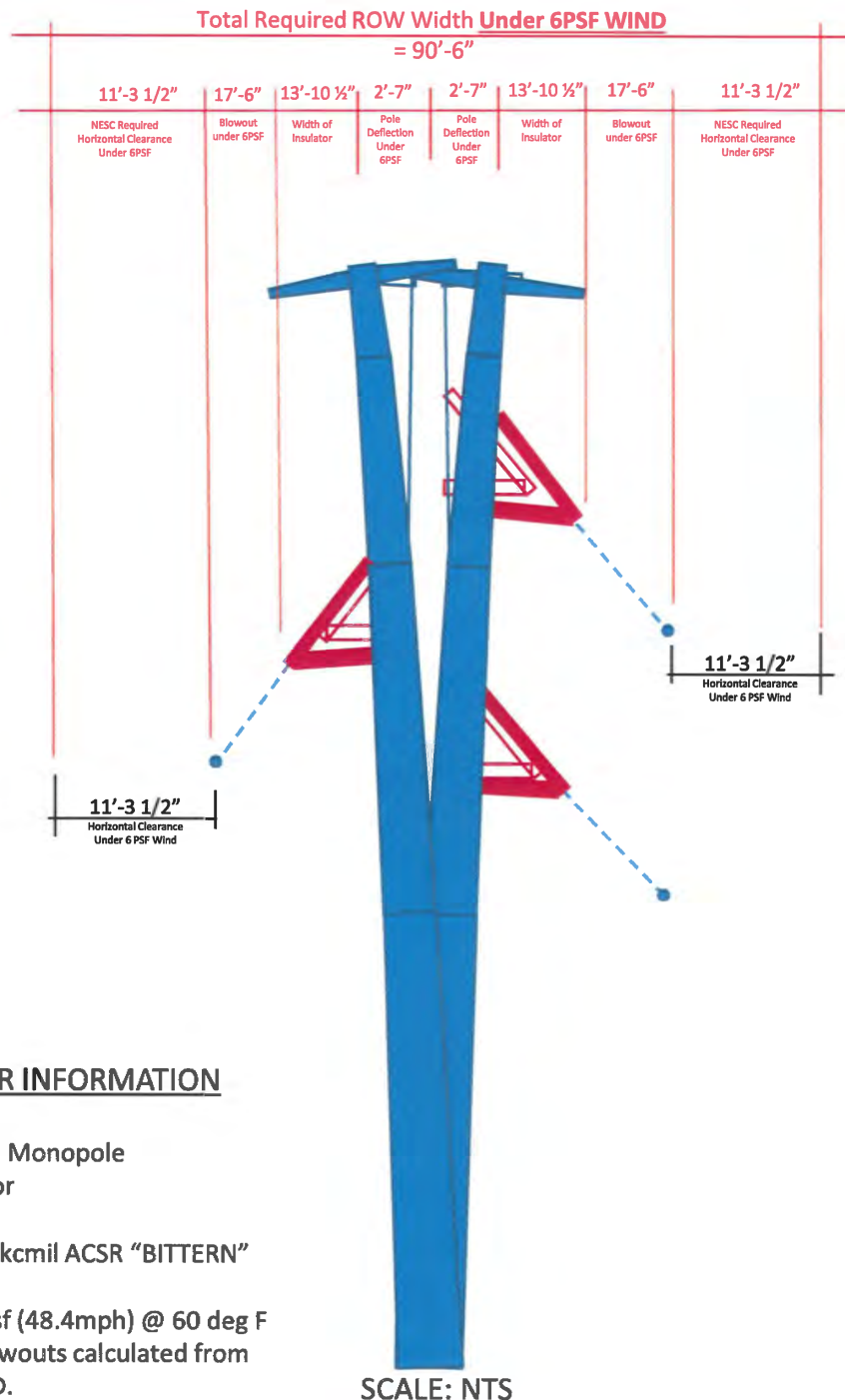


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 Approved By: G. PARENT
 Project Number:

SINGLE CIRCUIT STEEL
 MONOPOLE

DWG #: CCW-TRN-ROW-002 REVISION: C



STRUCTURE AND CONDUCTOR INFORMATION

Operational Voltage: 345kV
 Structure Type = Single Circuit Steel Monopole
 Insulator Type = Brace-Post Insulator
 Maximum Design Span = 1300ft
 Conductor Type = Bundled (2) 1272kcmil ACSR "BITTERN"
 NESC Rule Analyzed: 234B1b
 Weather Condition Displayed = 6 psf (48.4mph) @ 60 deg F
 Pole Deflections and Conductor Blowouts calculated from
 analysis of pole models in PLS-CADD.

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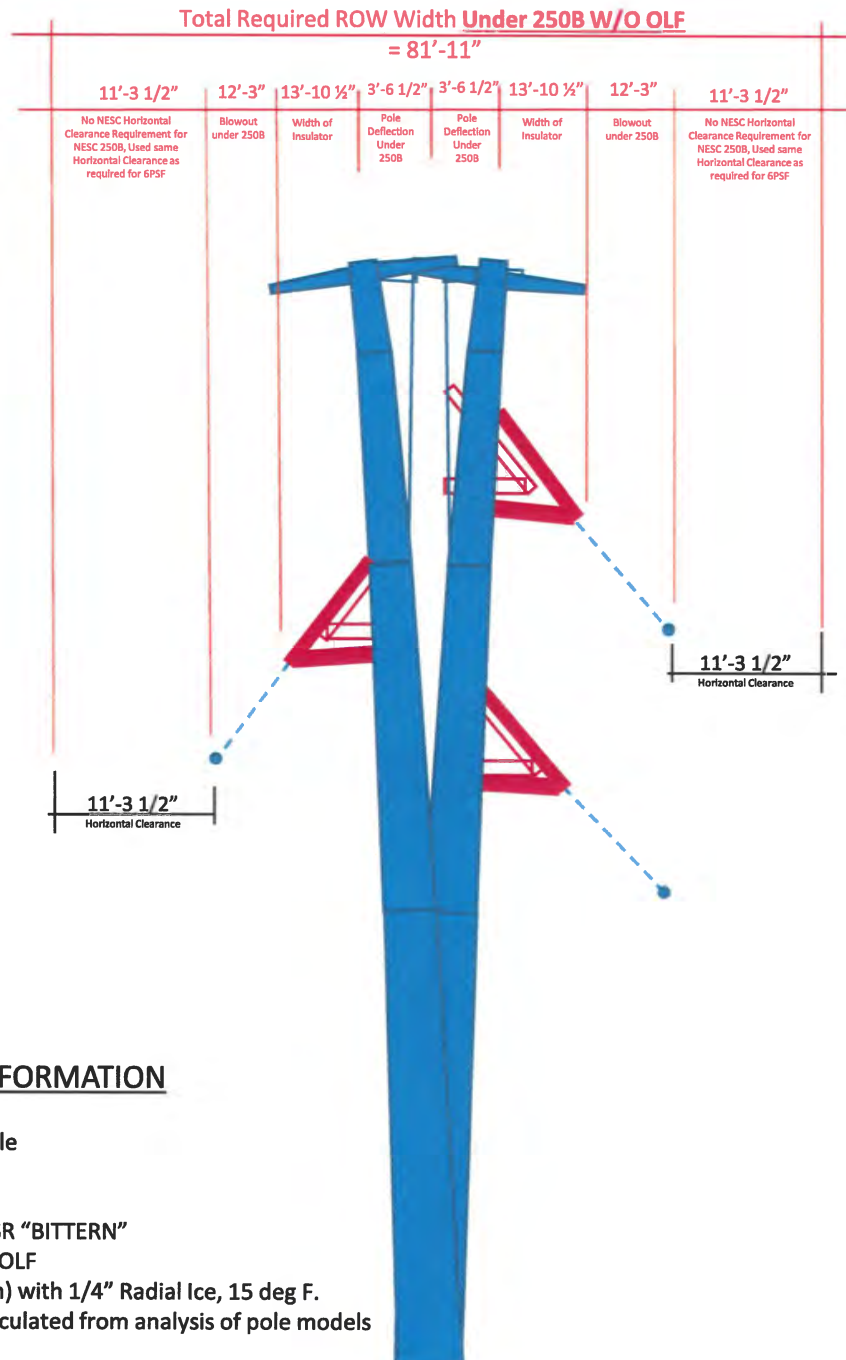


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 Drawn By: B. CAMPBELL
 Approved By: G. PARENT
 Project Number:

**SINGLE CIRCUIT STEEL
MONOPOLE**

DWG #: CCW-TRN-ROW-003 REVISION: C



STRUCTURE AND CONDUCTOR INFORMATION

Operational Voltage: 345kV

Structure Type = Single Circuit Steel Monopole

Insulator Type = Brace-Post Insulator

Maximum Design Span = 1300ft

Conductor Type = Bundled (2) 1272kcmil ACSR "BITTERN"

NESC Rule Analyzed: 250B – MEDIUM - W/O OLF

Weather Condition Displayed = 4 PSF (40mph) with 1/4" Radial Ice, 15 deg F.

Pole Deflections and Conductor Blowouts calculated from analysis of pole models in PLS-CADD.

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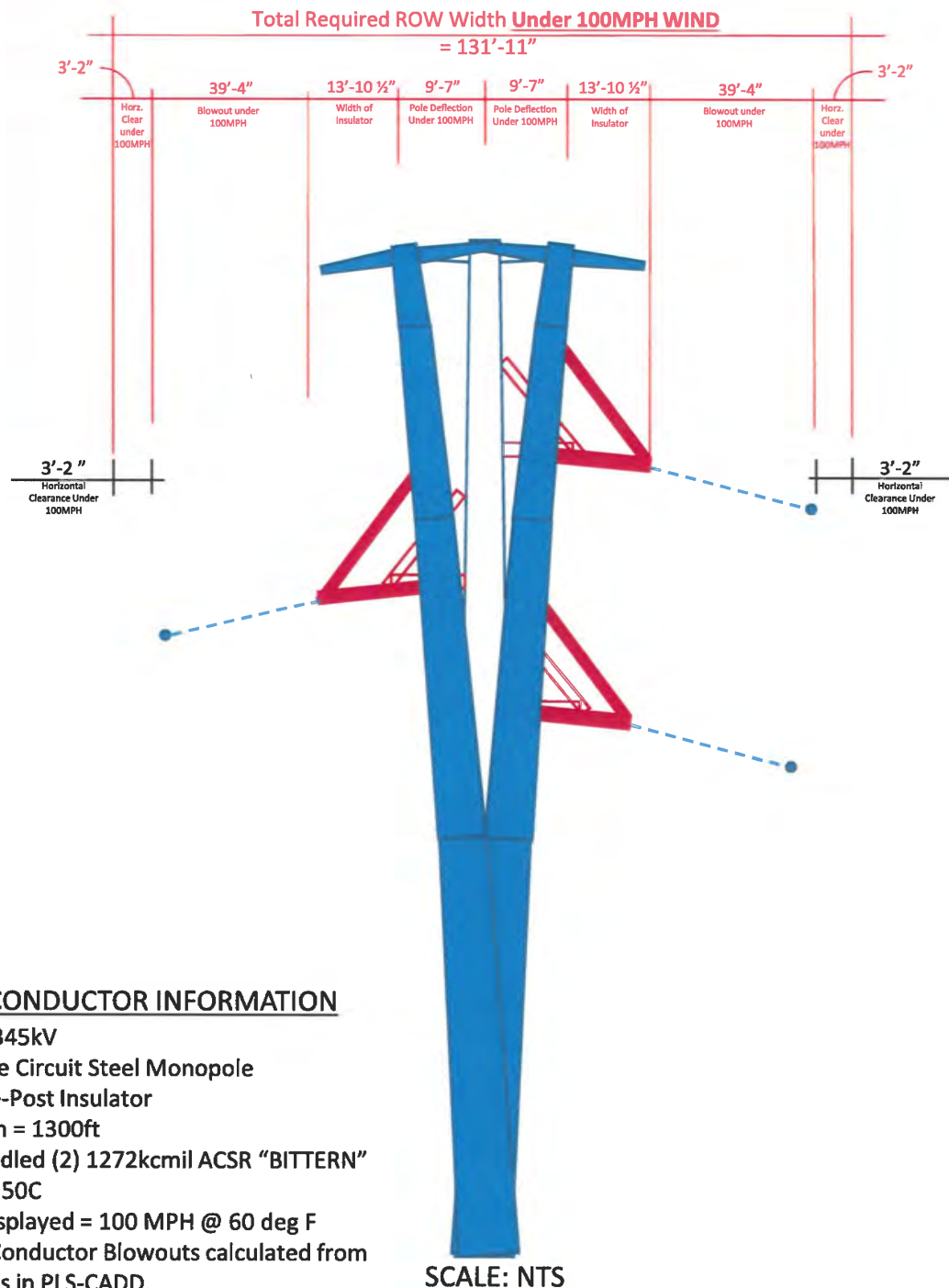
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Design By: G. PARENT
Drawn By: B. CAMPBELL
Approved By: G. PARENT
Project Number:

**SINGLE CIRCUIT STEEL
MONOPOLE**

DWG #: CCW-TRN-ROW-004
REVISION: C



STRUCTURE AND CONDUCTOR INFORMATION

Operational Voltage: 345kV
 Structure Type = Single Circuit Steel Monopole
 Insulator Type = Brace-Post Insulator
 Maximum Design Span = 1300ft
 Conductor Type = Bundled (2) 1272kcmil ACSR "BITTERN"
 NESC Rule Analyzed: 250C
 Weather Condition Displayed = 100 MPH @ 60 deg F
 Pole Deflections and Conductor Blowouts calculated from analysis of pole models in PLS-CADD.

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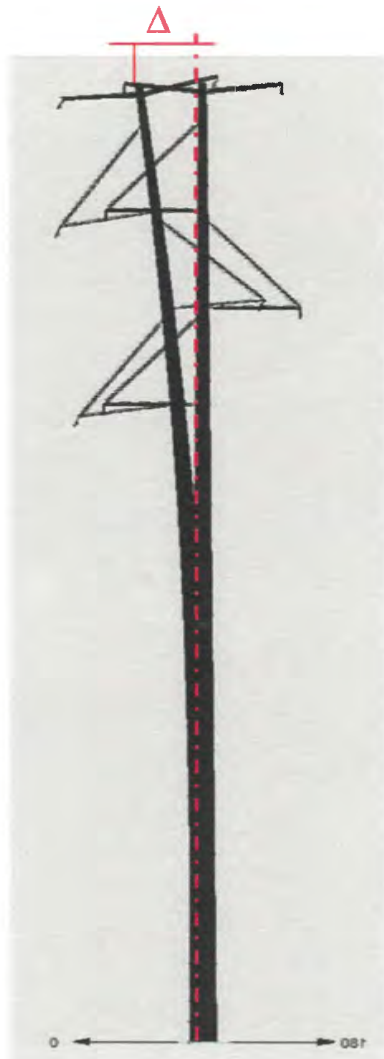


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 Approved By: G. PARENT
 Project Number:

**SINGLE CIRCUIT STEEL
MONOPOLE**

DWG #: CCW-TRN-ROW-005 REVISION: C



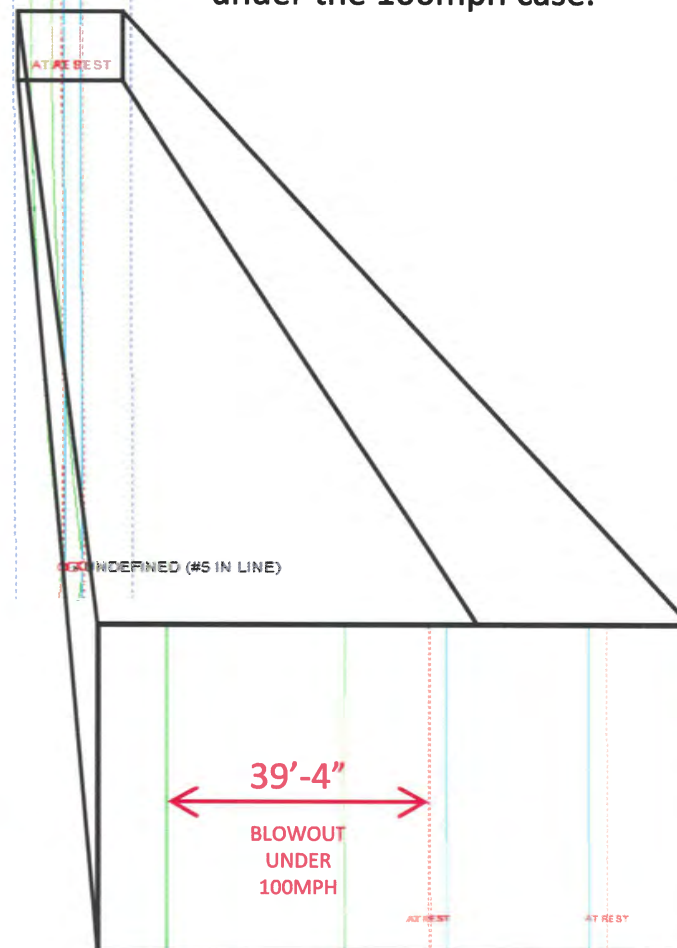
Summary of Tip Deflections For All Load Cases:

Note: positive tip load results in positive deflection

Load Case	Joint Label	Long. Defl. (in)	Trans. Defl. (in)	Vert. Defl. (in)	Resultant Defl. (in)	Long. Rot. (deg)	Trans. Rot. (deg)	Twist (deg)
DEFLECTION, NA+, I NA+	P:t	0.07	31.17	-0.47	31.17	0.00	-2.36	0.00
DEFLECTION, NA-, I NA-	P:t	0.07	-23.35	-0.26	23.39	0.00	1.47	-0.00
NESC 250B HEAVY NO OLF W/K, NA+, I NA+	P:t	0.07	42.69	-0.89	42.70	0.00	-3.41	0.00
NESC 250B HEAVY NO OLF W/K, NA-, I NA-	P:t	0.07	-28.57	-0.39	28.52	0.00	1.81	-0.00
NESC 250C EXTREME WIND, NA+, I NA+	P:t	0.08	114.74	-5.08	114.90	0.00	-8.20	0.00
NESC 250C EXTREME WIND, NA-, I NA-	P:t	0.08	-107.80	-5.12	107.92	0.00	7.41	-0.00

CONDUCTOR (#4 IN LINE)

This blowout calculation is for the maximum 1300ft Tangent to Tangent Spans. The figures to the left represent the PLS-CADD outputs for pole top deflections and the output for conductor blowout under the 100mph case.



CLINES CORNER WIND FARM TORRANCE COUNTY, NEW MEXICO

Rev.	Date	Description	By
A	03/02/19	PERMIT SUPPORT	UEI
B	05/03/19	REVISED	UEI
C	05/07/19	REVISED	UEI

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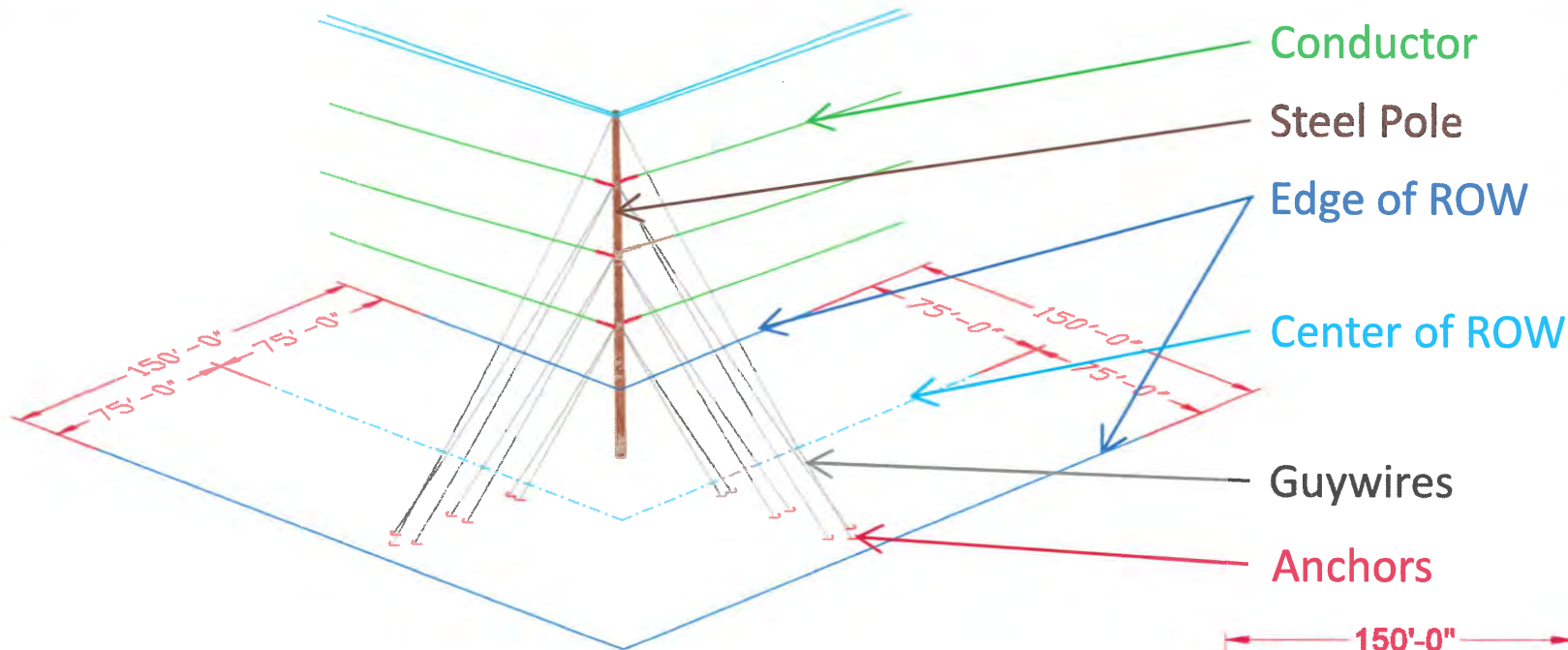


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Drawn By: B. CAMPBELL
Approved By: G. PARENT
Project Number:

TANGENT POLE TOP DEFLECTION AND CONDUCTOR BLOWOUT RESULTS

CCW-TRN-ROW-006

C



Isometric View of Guyed Heavy Angle

STRUCTURE AND CONDUCTOR INFORMATION

Operational Voltage: 345kV

Structure Type = Single Circuit Guyed Heavy Angle Monopole

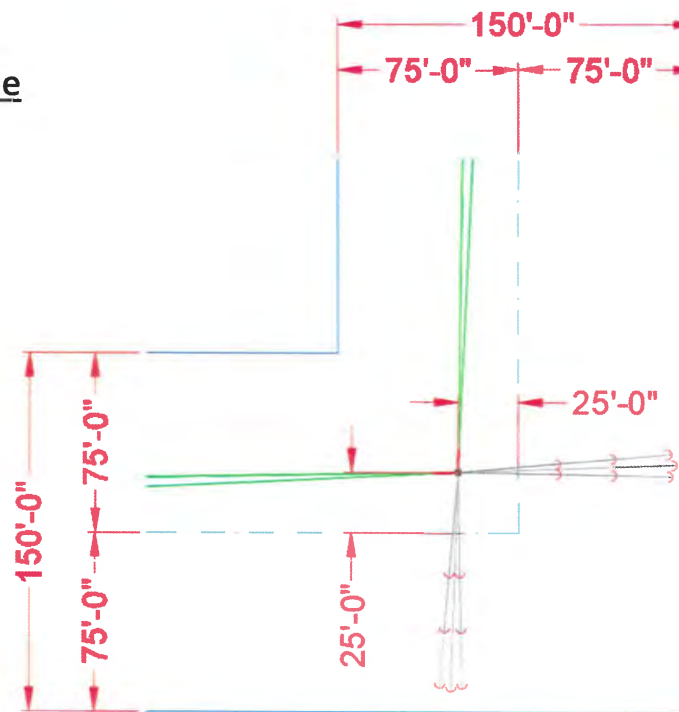
Insulator Type = Suspension Insulators

Typical Design Span = 800ft

Maximum Design Span = 1200ft

A guyed heavy angle monopole structure uses guywires to resist the lateral loads that are applied to the structure from the tensioned conductors. These guywires extend down at an angle from the pole structure to the groundline. Each guywire connects to an anchor structure.

To fit the "Guywire Footprint" in a 150ft ROW the pole structure is typically offset towards the inside edge of the ROW. Please see the drawings above and to the right which illustrate this structure/ROW geometry.



Plan View of Guyed Heavy Angle

CLINES CORNER
WIND FARM
TORRANCE COUNTY,
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Rev.	Date	Description	By
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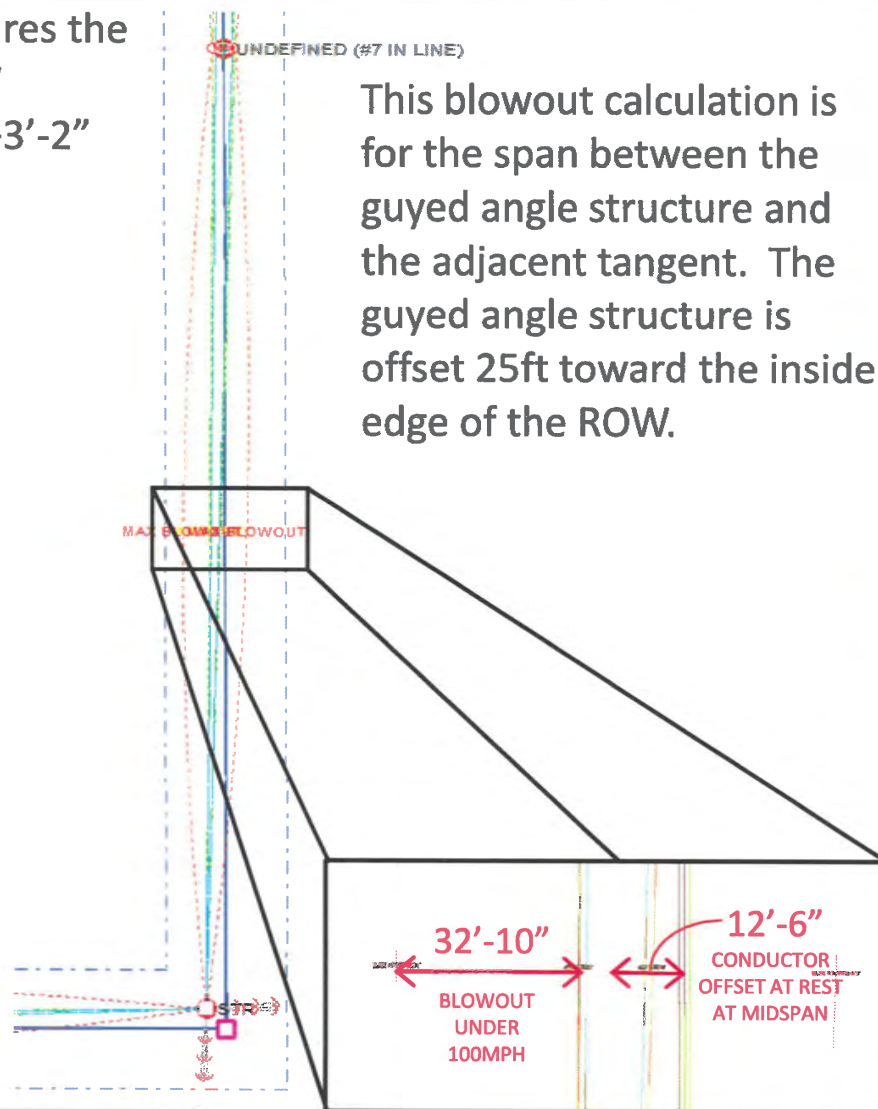
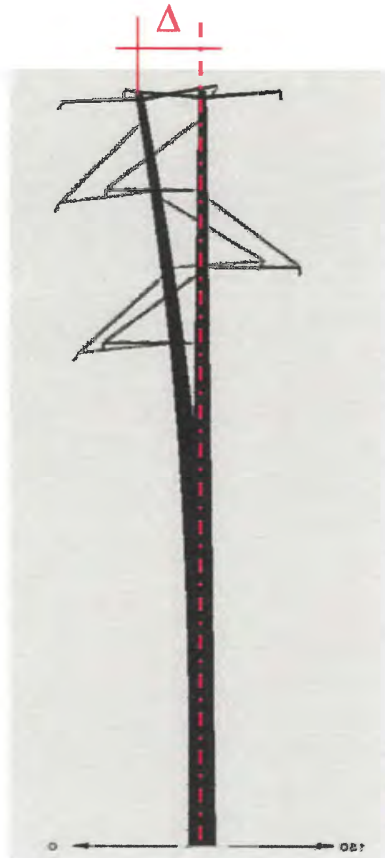
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Project Number:

**SINGLE CIRCUIT
GUYED HEAVY ANGLE
MONOPOLE**

DWG #: CCW-TRN-ROW-007 REVISION: C

For a 1200 ft span between these structures the
 Conductors Blowout from center of ROW
 $= 8'-9 \frac{1}{2}" + 12'-6" + 13'-10 \frac{1}{2}" + 32'-10" + 3'-2"$
 $= \underline{71'-2"} < \underline{75'-0"} \text{ O.K.}$

The spans
 between the
 guyed angles and
 the tangents will
 need to be
 limited to 1200ft
 to stay within the
 150ft ROW.



This blowout calculation is
 for the span between the
 guyed angle structure and
 the adjacent tangent. The
 guyed angle structure is
 offset 25ft toward the inside
 edge of the ROW.

Summary of Tip Deflections For All Load Cases:

Note: positive tip load results in positive deflection

Load Case	Joint Label	Long. Defl. (in)	Tran. Defl. (in)	Vert. Defl. (in)	Resultant Defl. (in)	Long. Rot. (deg)	Tran. Rot. (deg)	Twist (deg)
NESC 250C EXTREME WIND, NA+, I NA+	P:t	0.91	35.48	-4.97	105.60	0.07	-7.54	0.01
NESC 250C EXTREME WIND, NA-, I NA-	P:t	-0.63	-80.98	-2.87	81.03	-0.05	5.47	-0.01
NESC 250D ICE W/ WIND, NA+, I NA+	P:t	0.40	37.27	-0.67	37.28	0.03	-2.90	0.01
NESC 250D ICE W/ WIND, NA-, I NA-	P:t	-0.05	-10.54	-0.08	10.54	-0.00	0.53	-0.00
HEAVY ICE, I NA+	P:t	0.26	25.68	-0.39	25.68	0.02	-2.35	0.00
UPLIFT, I NA+	P:t	0.17	10.33	-0.08	10.33	0.01	-0.91	0.00
NESC RULE 261A (wind towards 192), I Max	P:t	-20.92	3.87	-0.20	21.28	-1.37	-0.25	0.00
DEFLECTION, NA+, I NA+	P:t	0.34	31.64	-0.48	31.64	0.02	-2.38	0.00
DEFLECTION, NA-, I NA-	P:t	-0.05	-13.16	-0.09	13.16	-0.00	0.74	-0.00

CLINES CORNER
 WIND FARM
 TORRANCE COUNTY,
 NEW MEXICO

Rev.	Date	Description	By
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 Drawn By: B. CAMPBELL
 Approved By: G. PARENT
 Project Number:

GUYED ANGLE POLE
 TOP DEFLECTION AND
 CONDUCTOR
 BLOWOUT RESULTS

CCW-TRN-ROW-008

C

Audible Noise Calculation For Typical Tangent

Project Name: Clines Corners Wind Project

Engineer: Greg Parent

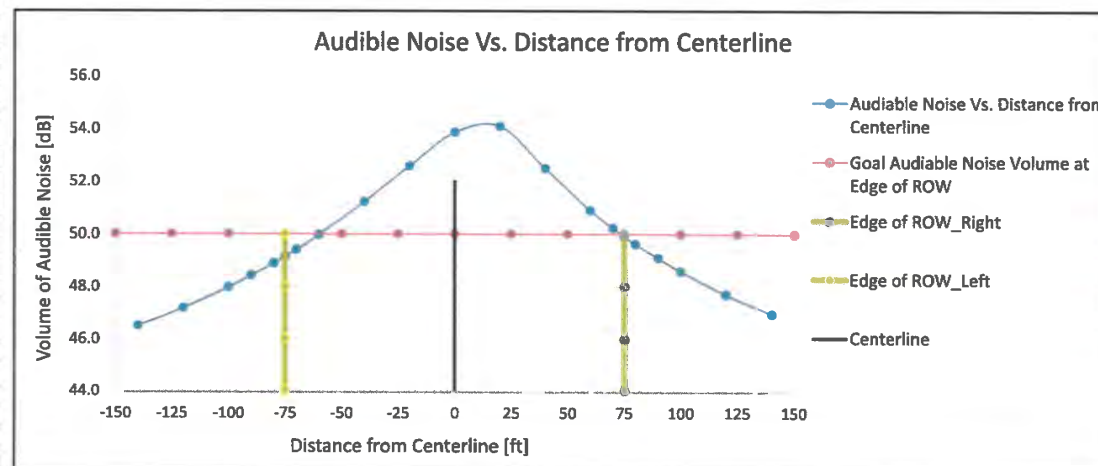
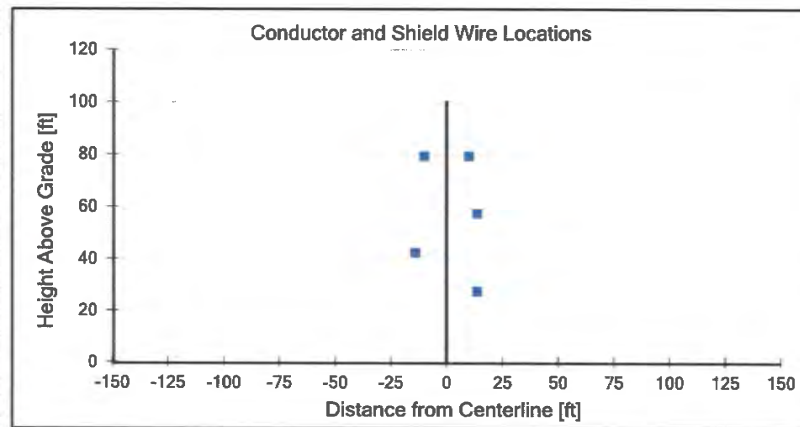


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Bundle	x-feet	y-feet	n cond	cond dia	spacing	l-n voltage	phase	Kv/cm
1	13.875	57.25	2	1.196	18	205	0	15.4498
2	-13.875	42.25	2	1.196	18	205	120	15.3010
3	13.875	27.25	2	1.196	18	205	240	16.0878
4	10	79.25	1	0.6		0	0	5.5614
5	-10	79.25	1	0.6		0	0	3.3127
6								0.0000
7								0.0000
8								0.0000

NPH= 5.00 Calculated Altitude ft= 6650
(Inverse 7995.91 Dummy Output) Note: Use "Paste Special" and "values" to copy data

Dist	L50 rain
Away from Center Line (ft)	Decibels at distance away from centerline [db]
-300	5 42.93 O.K.
-280	5 43.26 O.K.
-260	5 43.62 O.K.
-240	5 44.00 O.K.
-220	5 44.41 O.K.
-200	5 44.85 O.K.
-180	5 45.34 O.K.
-160	5 45.89 O.K.
-140	5 46.49 O.K.
-120	5 47.18 O.K.
-100	5 47.97 O.K.
-90	6 48.43 O.K.
-80	5 48.89 O.K.
-75	5 49.14 O.K.
-70	5 49.41 O.K.
-60	5 49.97 O.K.
-40	5 51.23 N.G.
-20	5 52.58 N.G.
0	5 53.86 N.G.
20	5 54.08 N.G.
40	5 52.49 N.G.
60	5 50.90 N.G.
70	5 50.23 N.G.
75	5 49.92 O.K.
80	5 49.63 O.K.
90	6 49.10 O.K.
100	5 48.58 O.K.
120	5 47.70 O.K.
140	5 46.95 O.K.
160	5 46.29 O.K.
180	5 45.71 O.K.
200	5 45.18 O.K.
220	5 44.71 O.K.
240	5 44.27 O.K.
260	5 43.87 O.K.
280	5 43.50 O.K.
300	5 43.16 O.K.



Max Decibels = 54.08

Goal: output in C column < 50 DB AT EDGE OF ROW

CLINES CORNER
WIND FARM
TORRANCE COUNTY,
NEW MEXICO

Rev.	Date	Description	By
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Approved By: G. PARENT
Project Number:

TANGENT
AUDIBLE NOISE AT
EDGE OF ROW

DWG #: CCW-TRN-ROW-009 REVISION: C

Audible Noise Calculation - Guyed Deadend

Project Name: Clines Corners Wind Project

Engineer: Greg Parent

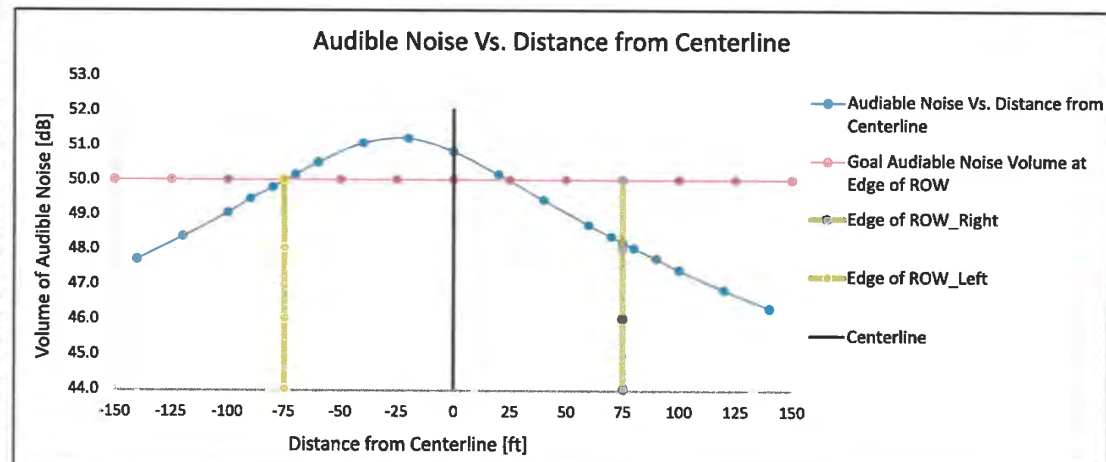
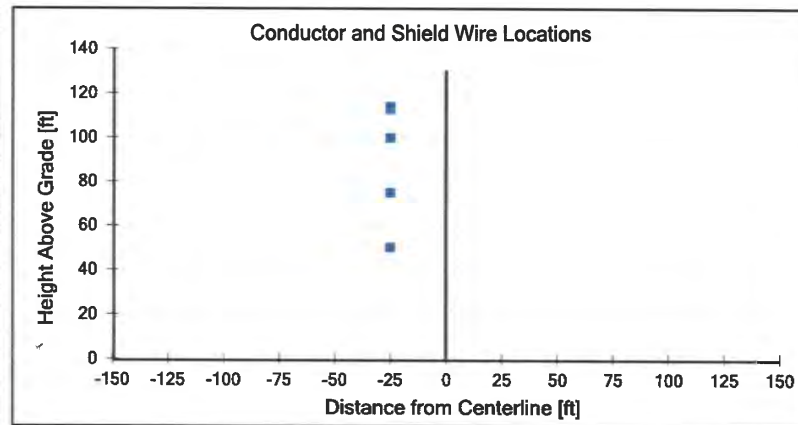
Bundle	x-feet	y-feet	n cond	cond dia	spacing	I-n voltage	phase	Kv/cm
1	-25	50	2	1.196	18	205	0	15.3505
2	-25	75	2	1.196	18	205	120	16.2685
3	-25	100	2	1.196	18	205	240	15.8528
4	-25	113	1	0.6		0	0	6.9300
5	-25	114	1	0.6		0	0	6.0427
6								0.0000
7								0.0000
8								0.0000

NPH= 5.00 Calculated Altitude ft= 6650
(Inverse 8023.79 Dummy Output) Note: Use "Paste Special" and "values" to copy data

Dist	L50 rain	
Away from Center Line (ft)	Decibels at distance away from centerline [db]	
-300	5	44.04 O.K.
-280	5	44.39 O.K.
-260	5	44.76 O.K.
-240	5	45.16 O.K.
-220	5	45.59 O.K.
-200	5	46.05 O.K.
-180	5	46.55 O.K.
-160	5	47.10 O.K.
-140	5	47.70 O.K.
-120	5	48.35 O.K.
-100	5	49.05 O.K.
-90	6	49.45 O.K.
-80	5	49.78 O.K.
-75	5	49.97 O.K.
-70	5	50.15 N.G.
-60	5	50.50 N.G.
-40	5	51.05 N.G.
-20	5	51.19 N.G.
0	5	50.81 N.G.
20	5	50.15 N.G.
40	5	49.41 O.K.
60	5	48.69 O.K.
70	5	48.35 O.K.
75	5	48.18 O.K.
80	5	48.02 O.K.
90	6	47.72 O.K.
100	5	47.39 O.K.
120	5	46.82 O.K.
140	5	46.30 O.K.
160	5	45.81 O.K.
180	5	45.37 O.K.
200	5	44.96 O.K.
220	5	44.57 O.K.
240	5	44.21 O.K.
260	5	43.88 O.K.
280	5	43.56 O.K.
300	5	43.26 O.K.

Max Decibels = 51.19

Goal: output in C column < 50 DB AT EDGE OF ROW



CLINES CORNER
WIND FARM
TORRANCE COUNTY,
NEW MEXICO

Rev.	Date	Description	By
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Drawn By: B. CAMPBELL
Approved By: G. PARENT
Project Number:

GUYED HEAVY ANGLE
AUDIBLE NOISE AT
EDGE OF ROW

DWG #: CCW-TRN-ROW-010 REVISION: C

BEFORE THE NEW MEXICO PUBLIC REGULATION COMMISSION

**IN THE MATTER OF THE APPLICATION FOR)
THE LOCATION OF THE CLINES CORNERS)
WIND FARM AND GEN-TIE SYSTEM IN)
TORRANCE AND GUADALUPE COUNTIES)
PURSUANT TO THE PUBLIC UTILITY ACT, NMSA)
1978, §§62-9-3 AND 62-9-3.2)**

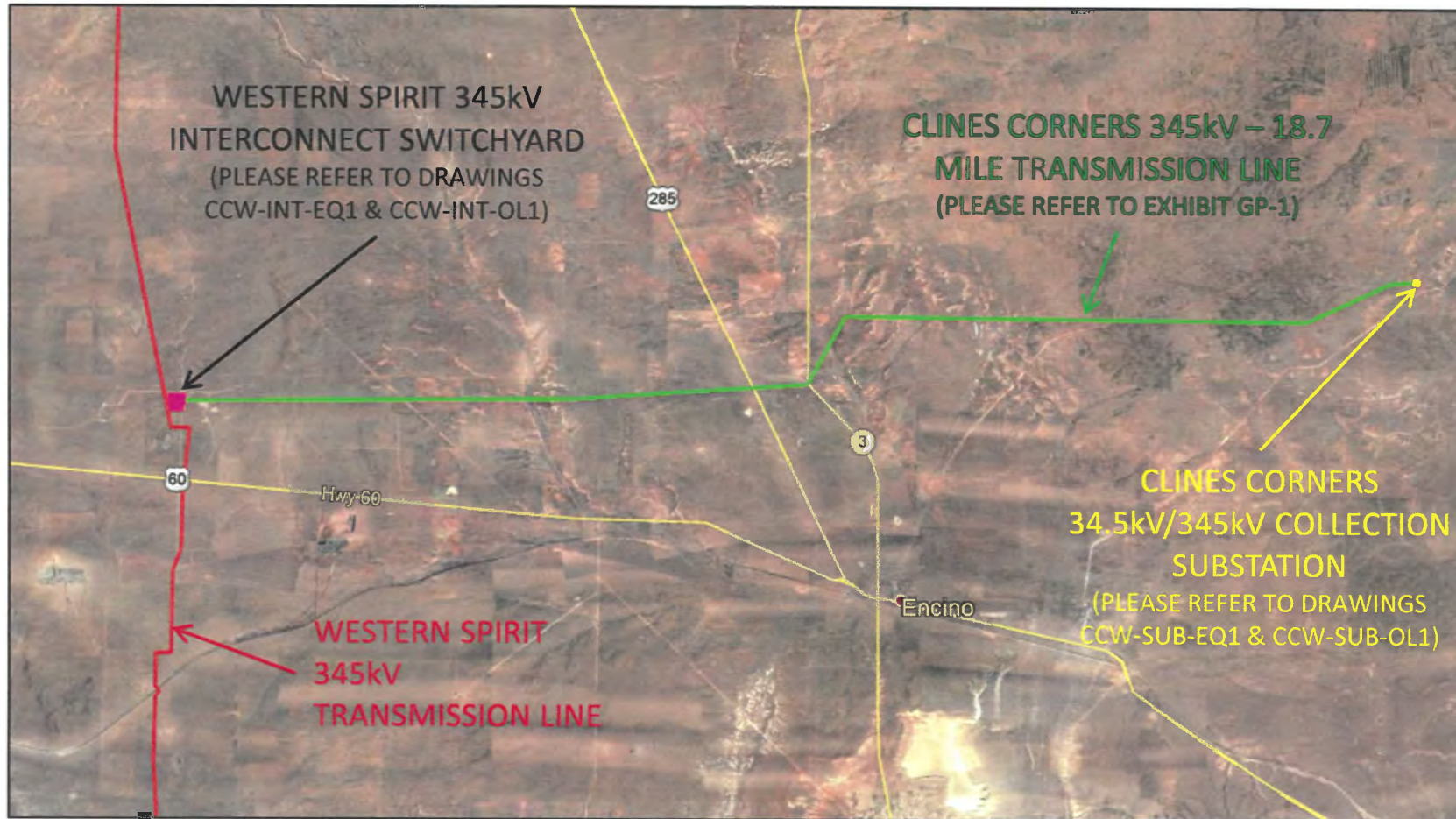
Case No. 19 - _____

CLINES CORNERS WIND FARM, LLC)

APPLICANT.)

EXHIBIT GP-2

CLINES CORNERS WIND FARM INTERCONNECTION WITH THE WESTERN SPIRIT 345KV TRANSMISSION LINE



CLINES CORNER
WIND FARM
TORRANCE COUNTY,
NEW MEXICO

Rev.	Date	Description	By
A	05/03/19	REVISED	UEI

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Exhibit GP-2

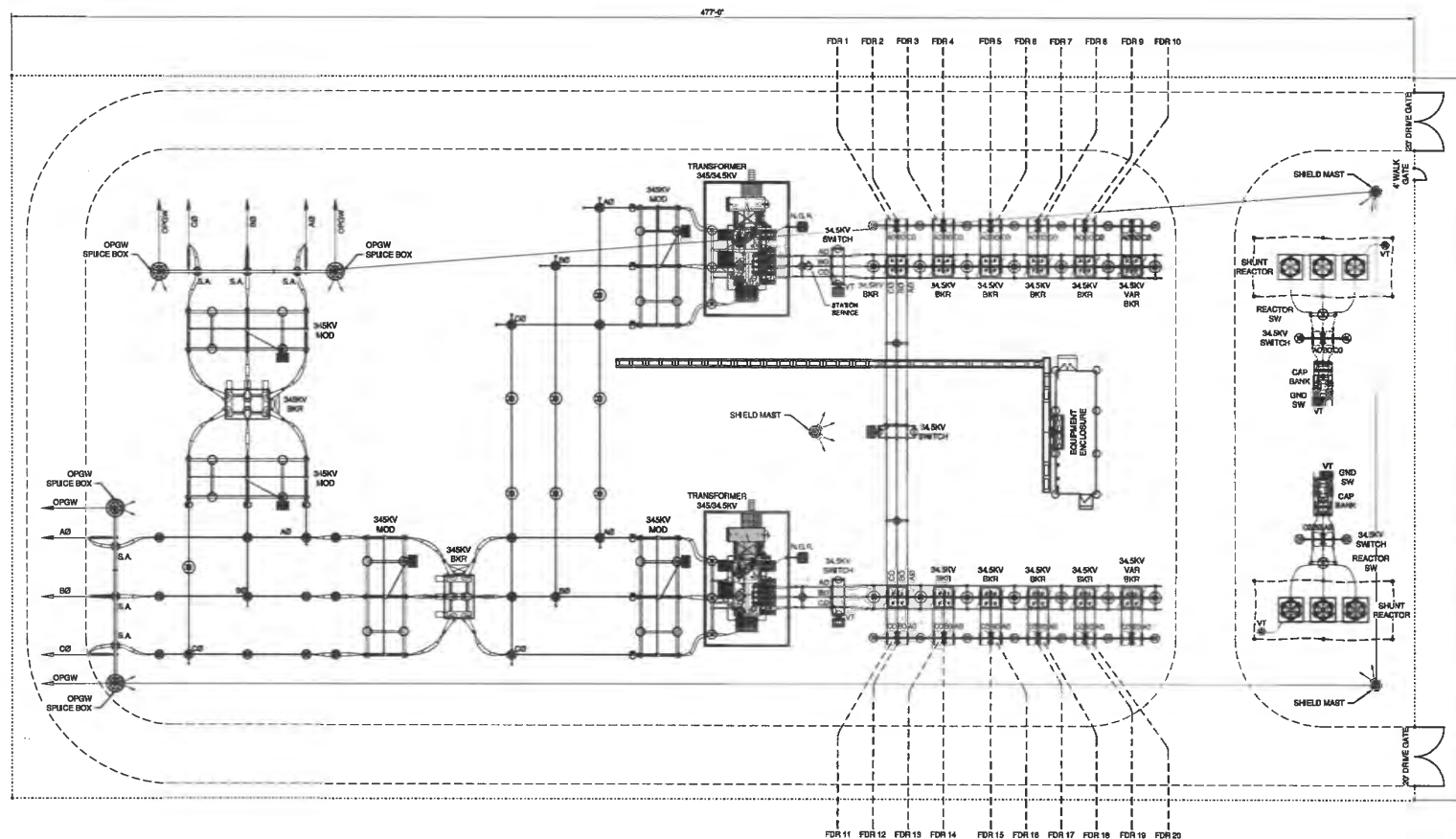
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Drawn By: B. CAMPBELL
Approved By: G. PARENT
Project Number:

CLINES CORNERS &
WESTERN SPIRIT
INTERCONNECTION MAP

DWG #: CCW-TRN-ICM
REVISION: A



CLINES CORNERS
WIND PROJECT
TORRANCE COUNTY,
NEW MEXICO

Rev	Date	Description	By
A	05/03/10	PRELIMINARY DESIGN PKG	UB

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LEGEND:

- OPERATOR PLATFORM
- INDICATES SECTION VIEW
- DRAWING ON WHICH SECTION APPEARS
- CABLE TRENCH
- AREA LIGHT
- BASE UNIDENTIFIED SECTION
- FENCE LINE



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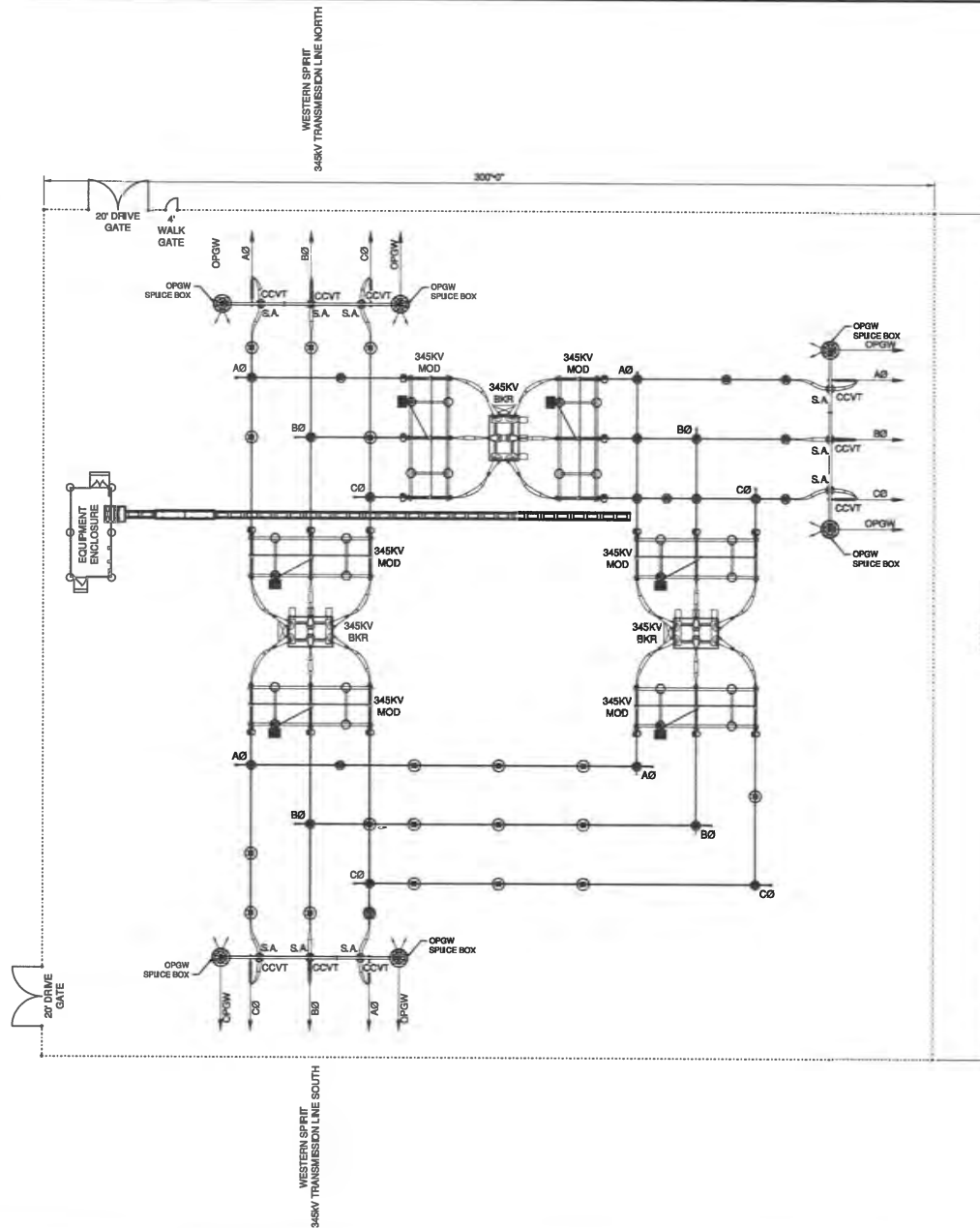
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Bentley - Owner - David Lutes - Fargo - State Falls - St. Paul
Design By: G. PARENT
Drawn By: B. CAMPBELL
Approved By:
Project Number: 18.05486

**SUBSTATION
GENERAL ARRANGEMENT**

REVISION:

A
DWG &
CCW-SUB-EQ1





CLINES CORNERS WIND PROJECT TORRANCE COUNTY, NEW MEXICO

Rev.	Date	Description	By
A	05/07/19	PRELIMINARY DESIGN PH3	US

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- DRAWING ON WHICH SECTION APPEARS
- CABLE TRENCH
- AREA LIGHT
- BASE LINE INTERSECTION
- FENCE w/ BARBS



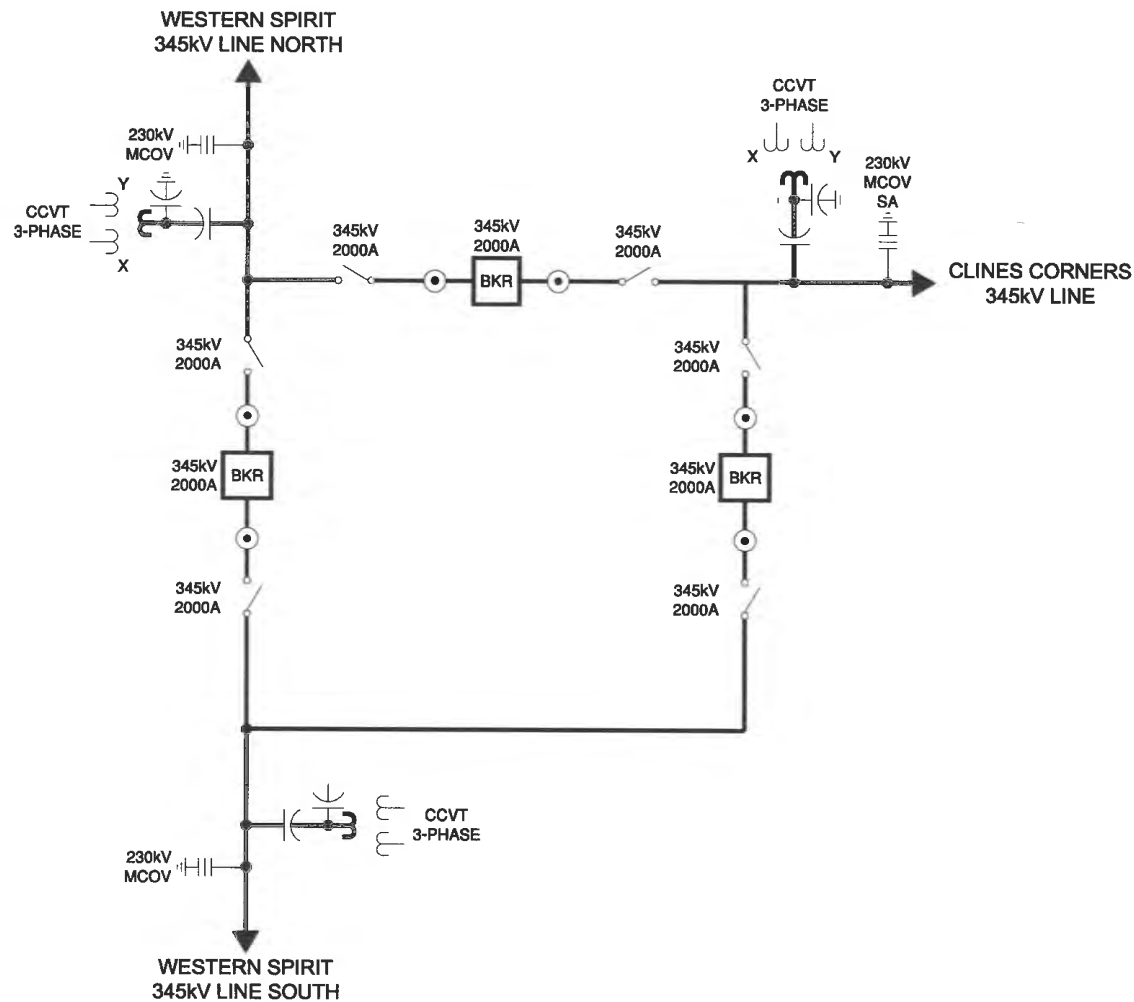
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Design By: G. PARENT
Drawn By: S. CAMPBELL
Approved By:
Project Number: 18-0048

SWITCH YARD GENERAL
ARRNG. (3) BREAKER RING
BUS INTERCONNECT
WITH WESTERN SPIRIT

REVISION:
A
DWG #
CCW-INT-EQ1



**CLINES CORNERS
WIND PROJECT
TORRANCE COUNTY,
NEW MEXICO**

Rev.	Date	Description	By
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Design By: G. PARENT
Drawn By: B. CAMPBELL
Approved By:
Project Number: 18.00498

**SWITCH YARD SWITCHING
DIAGRAM (3) BREAKER
RING BUS INTERCONNECT
WITH WESTERN SPIRIT**

REVISION:
A

CCW-INT-OL1

BEFORE THE NEW MEXICO PUBLIC REGULATION COMMISSION

**IN THE MATTER OF THE APPLICATION FOR)
THE LOCATION OF THE CLINES CORNERS)
WIND FARM AND GEN-TIE SYSTEM IN)
TORRANCE AND GUADALUPE COUNTIES)
PURSUANT TO THE PUBLIC UTILITY ACT, NMSA)
1978, §§62-9-3 AND 62-9-3.2)**

Case No. 19 - _____

CLINES CORNERS WIND FARM, LLC)

APPLICANT.)

AFFIDAVIT OF GREG PARENT

BEFORE THE NEW MEXICO PUBLIC REGULATION COMMISSION

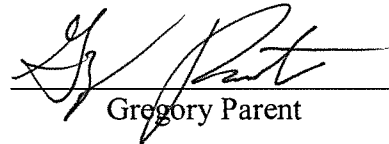
IN THE MATTER OF THE APPLICATION FOR)
THE LOCATION OF THE CLINES CORNERS)
WIND FARM AND GEN-TIE SYSTEM IN)
TORRANCE AND GUADALUPE COUNTIES)
PURSUANT TO THE PUBLIC UTILITY ACT, NMSA)
1978, §§62-9-3 AND 62-9-3.2)
CLINES CORNERS WIND FARM, LLC)
APPLICANT.)

Case No. 19 - _____

AFFIDAVIT OF GREGORY PARENT

STATE OF COLORADO)
COUNTY OF Arapahoe) ss.

I have read the foregoing Direct Testimony, and it is true and accurate based on my own knowledge and belief.


Gregory Parent

SUBSCRIBED and sworn to me before this 8th of May 2019.


NOTARY PUBLIC

December 14, 2022
My Commission Expires.

