

GRAND RENEWABLE ENERGY PARK WIND TURBINE SPECIFICATIONS REPORT

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Prepared for:

Samsung Renewable Energy Inc. 55 Standish Court Mississauga, ON L5R 4B2

Prepared by:

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#### **EXECUTIVE SUMMARY**

Samsung C&T (Samsung), Korea Power Electric Corporation (KEPCO) and Pattern Energy (Pattern) are proposing to develop, construct, and operate the Grand Renewable Energy Park (the "Project") in response to the Government of Ontario's initiative to promote the development of renewable electricity in the Province. Together, these companies (referred to herein as "SPK") will be involved in the development of the first phase of the energy cluster development.

The Project is proposed within the County of Haldimand and is generally bounded by Townline Road to the north, Haldimand Road 20 to the west, the Grand River to the east and Lake Erie to the south. It consists of a 151.1 MW (nameplate capacity) wind project, a 100 MW (nameplate capacity) solar project located on privately owned and Ontario Realty Corporation (ORC) managed lands and a transmission line to convey electricity to the existing power grid.

The basic components of the Project include 67 wind turbines, approximately 425,000 photovoltaic (PV) solar panels installed on fixed ground-mounted racking structures organized into 100-1 MW solar modules, a collector sub-station, interconnect station and Operations and Maintenance building, temporary storage and staging areas, approximately 20 km of 230 kV transmission lines along Haldimand Road 20, approximately 82 km of new overhead and/or underground 34.5 kV collector lines along public roads, approximately 48 km of new underground collector lines along turbine access roads, approximately 45 km of turbine access roads and 40 km of solar panel maintenance roads.

SPK has retained Stantec Consulting Ltd. (Stantec) to prepare a Renewable Energy Approval (REA) application, as required under Ontario Regulation 359/09 - Renewable Energy Approvals under Part V.0.1 of the Act of the *Environmental Protection Act* (O. Reg. 359/09). According to subsection 6(3) of O. Reg. 359/09, the wind component of the Project is classified as a Class 4 Wind Facility and the solar component of the Project is classified as a Class 3 Solar Facility. This Draft Wind Turbines Specification Report is one component of the REA application for the Project, and has been prepared in accordance with O. Reg. 359/09, and the Ontario Ministry of Natural Resources' (MNR's) *Approval and Permitting Requirements Document for Renewable Energy Projects* (September 2009).

The following table summarizes the documentation requirements as specified under O. Reg. 359/09.

Table E.1: Wind Turbine Specifications Report Requirements (as per O. Reg. 359/09 – Table 1)			
Requirements	Completed	Section Reference	
Provide specifications of each wind turbine, including make, model, name plate capacity, hub height above grade, rotational speeds and acoustic emissions data, including the sound power level and frequency spectrum, in terms of octave-band power levels.	✓	2.0	

The purpose of the Wind Turbine Specifications Report is to provide the public, aboriginal communities, municipalities, and regulatory agencies with an understanding of the technical specifications of the wind turbine generators to be utilized for the Project.

## **Table of Contents**

EXI	ECUTIVE SUMMARY	E.1
1.0	OVERVIEW	1.1
2.0	TECHNICAL SPECIFICATIONS	2.1
2.1	SWT-2.3-101 WIND TURBINE	2.1
2.2	WIND TURBINE LOCATIONS	2.1
3.0	CLOSURE	

### List of Tables

|--|

#### **List of Attachments**

Attachment A Turbine Specifications Attachment B Turbine Locations

#### 1.0 Overview

Samsung C&T (Samsung), Korea Power Electric Corporation (KEPCO) and Pattern Energy (Pattern) are proposing to develop, construct, and operate the Grand Renewable Energy Park (the "Project") in response to the Government of Ontario's initiative to promote the development of renewable electricity in the Province. Together, these companies (referred to herein as "SPK") will be involved in the development of the first phase of the energy cluster development.

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#### 2.0 Technical Specifications

#### 2.1 SWT-2.3-101 WIND TURBINE

The Project includes 67 Siemens SWT-2.3-101 wind turbines (65 turbines with a nameplate capacity of 2.221 MW and 2 turbines with a nameplate capacity of 2.126 MW). All physical attributes of the turbine remain the same however the reduction of name plate capacity impacts the maximum power output of the turbine as well as each turbines noise characteristics.

A summary of the basic specifications of the turbine model is provided in Table 2.1 below. A complete description of the general specifications for this turbine model is found in the manufacturer's information provided as **Attachment A**.

Table 2.1: Turbine Description – Siemens SWT-2.3		
Operating Data	Specification	
General		
Rated capacity (kW)	2221 and 2126	
Cut-in wind speed (m/s)	3-5	
Cut-out wind speed (m/s)	25	
Rotor		
Number of rotor blades	3 (49 m long each)	
Rotor diameter (m)	101	
Swept area (m <sup>2</sup> )	8000	
Rotor speed (rpm)	6-16	
Tower		
Hub height (m)	100	
Tip height (m)	149	

Acoustic emissions data supplied by Siemens is provided in **Attachment A.** Additional acoustic data is also provided in the Environmental Noise Impact Assessment contained within the Design and Operations Report.

#### 2.2 WIND TURBINE LOCATIONS

The wind turbines will be located at the locations and coordinates provided in **Attachment B**. The map also identifies the 2 turbines that have a nameplate capacity of 2.126 MW.

#### 3.0 Closure

This report has been prepared by Stantec for the sole benefit of SPK, and may not be used by any third party without the express written consent of SPK. The data presented in this report are in accordance with Stantec's understanding of the Project as it was presented at the time of reporting.

This Turbine Specifications Report has been prepared in accordance with O. Reg. 359/09. The data presented in this report are in accordance with Stantec's understanding of the Project as it was presented at the time of the Report.

#### STANTEC CONSULTING LTD.



Mark Kozak Project Manager

Rob Nadolny Senior Project Manager

# **Attachment A**

## **Turbine Specifications**

# WINDTEST Kaiser-Wilhelm-Koog GmbH

#### Report of acoustical emissions of a Siemens wind turbine generator system of the type 2.3 MW Mk II near Høvsøre in Denmark

Date(s) of measurements: 2005-08-11 to 13

September 2005

**Report WT 4498/05** 



Laboratory accredited by DAP Deutsches Akkreditierungssystem Prüfwesen according to DIN EN ISO/IEC 17025. This accreditation is valid for the test and measurement procedures given in the certificate.







#### Report of acoustical emissions of a Siemens wind turbine generator system of the type 2.3 MW Mk II near Høvsøre in Denmark

#### Report WT 4498/05

Site or measuring place:	Høvsøre, Denmark in the region of Ringkøbing	
Customer:	Siemens Wind Power A/S Borupvej 16	
	7330 Brande, Denmark	

Contractor:	WINDTEST Kaiser-Wilhelm-Koog GmbH Sommerdeich 14 b 25709 Kaiser-Wilhelm-Koog, Germany
	20700 Raiser-willenn-Roog, Germany

Date of order:	2005-08-23	Order No.:	4025 05 03069 64
Engineer:	]		Checked:

A. Jensen Dipl

. Neulf

Dipl.-Ing. J. Neuber Acoustics Group Leader

Kaiser-Wilhelm-Koog, 2005-09-08



#### **Table of contents**

1		Scope	. 4
2		Method	. 4
	2.1	Measurement procedures	.4
	2.2	Measurement object	.4
	2.3	Course of the measurements	.4
	2.4	Measuring equipment	. 5
	2.5	Position of microphone	. 5
3		Measurement results	. 5
	3.1	Determination of directivity	. 5
	3.2	Sound pressure level	. 6
	3.3	Sound power level of the turbine	. 7
	3.4	Tonal and frequency analyses	. 7
	3.5	3rd octave analysis	. 8
	3.6	Uncertainties	. 9
	3.6. 3.6. 3.6.	1 Sound power level 2 One-third octave band spectra 3 Tonality	. 9 10 10
4		Summary1	10
5		List of employed symbols and abbreviations1	12
6		References1	13
7		Annex 1	13
	Ann	ex 1: Measuring equipment used1	4
	Ann	ex 2.1a: $2^{nd}$ order regression of L <sub>Aeq</sub> and L <sub>n</sub> against standardised wind speed1	15
	Ann	ex 2.1b: Higher order regression of $L_{Aeq}$ and $L_n$ against standardised wind speed1	6
	Ann	ex 2.2: Summary of analysis input parameters and results1	17
	Ann	ex 2.3: Plot of L <sub>WA</sub> against standardised wind speed1	8
	Ann	ex 2.4: Plot of $L_{Aeq}$ and $L_n$ against measured wind speed	9
	Ann	ex 2.5: Plot of L <sub>Aeq</sub> against power2	20
	Ann	ex 2.6: Plot of rotor speed against power2	21
	Ann	ex 2.7: Time plot of measurement2	22
	Ann	ex 3.1a: Overview spectra 1-6 of turbine noise at a wind speed of 6 m/s	23
	Ann	ex 3.1b: Overview spectra 7-12 of turbine noise at a wind speed of 6 m/s	24
	Ann	ex 3.1c: Analysis of tonality of turbine noise at a wind speed of 6 m/s2	25
	Ann	ex 3.2a: Overview spectra 1-6 of turbine noise at a wind speed of 7 m/s	26





Annex 3.2b: Overview spectra 7-12 of turbine noise at a wind speed of 7 m/s
Annex 3.2c: Analysis of tonality of turbine noise at a wind speed of 7 m/s
Annex 3.3a: Overview spectra 1-6 of turbine noise at a wind speed of 8 m/s
Annex 3.3b: Overview spectra 7-12 of turbine noise at a wind speed of 8 m/s 30
Annex 3.3c: Analysis of tonality of turbine noise at a wind speed of 8 m/s
Annex 3.4a: Overview spectra 1-6 of turbine noise at a wind speed of 9 m/s
Annex 3.4b: Overview spectra 7-12 of turbine noise at a wind speed of 9 m/s
Annex 3.4c: Analysis of tonality of turbine noise at a wind speed of 9 m/s
Annex 3.5a: Overview spectra 1-6 of turbine noise at a wind speed of 10 m/s
Annex 3.5b: Overview spectra 7-12 of turbine noise at a wind speed of 10 m/s
Annex 3.5c: Analysis of tonality of turbine noise at a wind speed of 10 m/s
Annex 4.1: A-weighted sound pressure 1/3-octave spectrum at 6 m/s
Annex 4.2: A-weighted sound pressure 1/3-octave spectrum at 7 m/s
Annex 4.3: A-weighted sound pressure 1/3-octave spectrum at 8 m/s
Annex 4.4: A-weighted sound pressure 1/3-octave spectrum at 9 m/s
Annex 4.5: A-weighted sound pressure 1/3-octave spectrum at 10 m/s
Annex 5: Photos
Annex 6: Power curve used in the analysis45
Annex 7a: Manufacturer's certificate, page 1/246
Annex 7b: Manufacturer's certificate, page 247



#### 1 Scope

The order from Siemens Wind Power A/S dated 2005-08-23 required WINDTEST Kaiser-Wilhelm-Koog GmbH (WINDTEST) to carry out acoustic noise measurements on the Siemens wind turbine generator system (WTGS or 'turbine') 2.3 MW Mk II of hub height 80 m near Høvsøre, in the region of Ringkøbing in Denmark. From this, the sound power level, relevant for noise propagation calculations, of the noise emitted from the turbine at different wind speeds, and frequency spectra of the same, was also to be determined.

The results given in this report relate only to this WTGS.

#### 2 Method

#### 2.1 Measurement procedures

All measurements and analysis described in this report were done in accordance with the IEC 61400-11: Wind turbine generator systems – Part 11: Acoustic noise measurement techniques, Ed. 2 [IEC 61400-11] using Method 1 as outlined in 7.3.1.1 "Method 1: determination of the wind speed from the electric output and the power curve". In this report the sound power level and the tonality are given in the range of wind speeds from 6 to 10  $^{m}/_{s}$  at a height of 10 m.

**Note:** A calculated power curve for the turbine was provided by the customer for purposes of converting the measured turbine power output into the standardised wind speed. This power curve is given in the Annex.

#### 2.2 Measurement object

Table 1 shows the characteristics of the measured WTGS. The remaining characteristics can be found in the manufacturer's certificate included in the Annex.

parameter	Value
manufacturer	Siemens Wind Power A/S
type	2.3 MW Mk II
WTGS No.	2300439
site	Høvsøre, Denmark
hub-height above ground	80 m
rotor diameter	92,4 m
distance middle of tower to middle of blade flange	3,5 m
power control (pitch/stall)	pitch

 Table 1: Characteristics of the measured WTGS

#### 2.3 Course of the measurements

The total measurement period lasted from 2005-08-12 15:00 h until 2005-08-13 20:00 h. During this time the measured wind speed ranged from 5,5 to 12 m/s at a height of 10 m. The real



electrical power output of the turbine ranged between 300 and 2300 kW. The turbine was running continuously during the operating noise measurements.

The sound pressure level was recorded with a microphone on an acoustically hard board. The real electrical power output and the wind speed at a height of 10 m, taken upwind of the turbine in clear air, were also recorded. Time periods, where there were intermittent background noise of a significant nature, e.g. passing cars, planes flying over, rain etc., were marked accordingly during the measurements, and were omitted in the later evaluation. If there were random and reoccurring disturbances, which could not be marked during the measurement, a later state correction by means of a comparison with the DAT-recording was done.

The wind turbine generator system is sited in farmland. The surface roughness length for this measurement is assumed to be 0.05 m. The microphone position was chosen to minimise the effect of buildings, trees or bushes in the surrounding area of the wind turbine generator system, which might have had an influence on the measurement results. The conditions comply with free field behaviour over a reflecting plane.

During the noise measurements the meteorological conditions given in Table 2 were prevailing.

barometric pressure at 2 m height above ground [hPa]	1001 - 1006
air temperature at 2 m height above ground [°C]	14 - 18
prevailing wind direction	WNW
range of wind direction	280 - 330
weather conditions	cloudy and dry
<i>Turbulence intensity at 10 m height above ground [%]</i>	14,0

Table 2: Prevailing meteorological conditions during the measurements

#### 2.4 Measuring equipment

The measuring equipment used is listed in the Annex. This equipment is tested regularly according to [IEC 61400-11] to ensure a high degree of measurement accuracy as well as security of data. The complete acoustic measurement system was checked before and after the measurements using an acoustic calibrator (B&K 4231).

#### 2.5 **Position of microphone**

The microphone was placed according to [IEC 61400-11]. The distance from the turbine to the reference measuring point,  $R_0 = 112$  m, was chosen taking local circumstances into account. The height of the microphone with respect to the bottom of the turbine foundation was 0 m.

#### 3 Measurement results

#### 3.1 Determination of directivity

As no significant directivity was ascertained the reference measurement position was chosen to be directly downwind of the turbine. This ensured worst case sound propagation conditions were taken into account.



#### 3.2 Sound pressure level

The microphone converts the sound pressure into a continuous analogue signal which is then fed to a sound level meter. The resulting dB value,  $L_{Aeq}$ , together with the status, the wind speed at a height of 10 m, WS, and the real power output of the turbine,  $P_{w}$ , all recorded by the measurement system, is plotted against time in a graph given in the Annex. Here it can be seen at which points in time the turbine is switched on and off and provides an overview of the background noise in relation to the operating noise recorded by the measurement system over the whole period of the measurement. As can be seen, data was captured continuously throughout the whole measurement period. Non-normal background noises occurring in the measurement period, e.g. from aircraft or traffic, were marked during data acquisition to enable their easy omission in the evaluation to follow. The state signal is used to differentiate between periods when the turbine is running and when it is stopped. *State* = 3 depicts a running turbine, *state* = 0.5 depicts a stopped turbine, and *state* = 0 marks the data to be omitted in the evaluation.

The noise produced by the turbine alone  $L_{Aeq,c}$  at wind speeds of 6, 7, 8, 9 and 10 m/s is then determined by converting the dB levels of background and in-service noise to intensities, performing a subtraction and converting back again to dB. In order to determine this, regression curves of the measured sound pressure level with the turbine both running and stopped, plotted with respect to the standardised wind speed at a height of 10 m are required. The wind speed measured during the background noise measurement is multiplied by the factor  $\kappa$ , which is defined as the following:

$$\kappa = \frac{V_s}{V_z}$$

where,

 $V_s$  is the standardised wind speed

 $V_r$  is the measured wind speed.

For this measurement,  $\kappa = 0.93$ .

The results of this regression analysis are given in the Annex. All relevant sound pressure level values are given in the annex.

**Remark:** The data have been analysed using a fourth order regression because this is the best fitting approximation through all the relevant data points. In accordance with [IEC 61400-11] the data have also been analysed using a second order regression which is given in the annex only for information purposes. The sound levels resulting from the higher order regression have been applied in the third octave analysis.



#### 3.3 Sound power level of the turbine

In accordance with [IEC 61400-11] the sound power level  $L_{WA,k}$  of the turbine in dB is derived from the corrected sound pressure level  $L_{Aeq,c,k}$ , at wind speeds between 6 and 10 m/s at a height of 10 m, using the following formula:

$$L_{WA,k} = L_{Aeq,c,k} - 6 + 10 \cdot \lg \left(\frac{4 \cdot \pi \cdot R_1^2}{S_0}\right)$$

where, 6 dB is the correction due to the doubled sound pressure sensed by the microphone caused by coherent interference at the acoustically hard board.

 $10 \cdot lg\left(\frac{4 \cdot \pi \cdot R_1^2}{S_0}\right)$  = the ratio in dB of the surface area of a sphere having the radius  $R_1$ 

to the reference surface area of  $S_0$ 

where,

$$S_0 = 1 \text{ m}^2$$
  
 $R_1 = \sqrt{(R_0 + d)^2 + (H - h_A)^2}$ 

 $R_0$  = distance between tower centre and microphone position

d = distance between tower centre and rotor flange middle point

H = hub-height above ground level

 $h_A$  = height of microphone

The following results are given in the Annex:

- A graph showing regressions through all the measured wind turbine sound data  $L_{\text{Aeq}}$  and background noise data  $L_{n}.$
- A plot of the background corrected normalised values of L<sub>WA</sub> against the standardised wind speed.
- A plot of L<sub>Aeq</sub> and L<sub>n</sub> against measured wind speed.
- A plot of L<sub>Aeq</sub> against power.
- A plot of rotor speed against power.
- A time plot of the measurement.

For the Siemens 2.3 MW Mk II in the present configuration the real power output and the apparent sound power levels are given in table 4.

#### 3.4 Tonal and frequency analyses

In accordance with the technical guideline [IEC 61400-11] a tonal analysis has to be carried out. The frequency spectrum of the noise, which is measured on the acoustically hard board, is determined on the basis of a narrow band analysis by means of the FFT-analyser B&K 2144. This analysis was performed after the measurements using the audio signal recorded on a DAT-recorder.



The results of the tonal analysis of the Siemens 2.3 MW Mk II according to [IEC 61400-11] are given in table 4.

#### 3.5 3rd octave analysis

The A-weighted sound spectra at all the integer wind speeds are given in the Annex.



#### 3.6 Uncertainties

#### 3.6.1 Sound power level

The result of the sound power level measurement is subject to uncertainties which are due to the environment, meteorological conditions and the measurement system. For these measurements all the type B measurement uncertainty components as specified in the technical guideline [IEC 61400-11] are given in Table 3. For all of the type B uncertainties mentioned here, a rectangular distribution of possible values is assumed for simplicity with a range described as "±a". The standard deviation for such a distribution is:

$$U = \frac{a}{\sqrt{3}}$$

Component	Range [dB]	Uncertainty [dB]
Calibration, $U_{B1}$	±0,2	0,12
Chain of acoustic measurement instruments, $U_{B2}$	±0,4	0,23
Acoustically hard board, $U_{B3}$	±0,5	0,29
Distance measurement, $U_{B4}$	±0,1	0,06
Acoustic impedance of air, $U_{B5}$	±0,2	0,12
Meteorological variation (including turbulence), $U_{\rm B6}$	±0,7	0,40
Wind speed derived from the power curve, $U_{\scriptscriptstyle B7}$	±0,3	0,17
Wind direction, $U_{BB}$	±0,5	0,29
$\sum_{i=1}^{8} U_{Bi}^{2}$		0,44

Table 3: Type B measurement uncertainty components

The error in the background correction  $U_{B9}$  in dB has been calculated for each integer wind speed as follows:

$$U_{B9} = L_{Aeq,c,k} - \left[10 \cdot \log\left(10^{0,1 \cdot L_{Aeq,k}} - 10^{0,1(L_n + U_{HG})}\right)\right]$$

where  $U_{\rm HG}$  is the error in the background noise in dB defined as follows:



$$U_{\rm HG} = \sqrt{\frac{\left(y_n - y_{n,est}\right)^2}{N_n - 2}}$$

where:

$$y_n$$
 = measured sound pressure level of background noise in dB

$$y_{n,est}$$
 = estimated sound pressure level of background noise from the regression analysis  
in dB

$$N_n$$
 = number of background noise measurement values in the wind speed bin corresponding to the integer wind speed.

The combined measurement uncertainty  $U_c$  relating to the sound power level  $L_{WAK}$  is calculated as follows:

$$U_{C} = \sqrt{U_{A}^{2} + U_{B9}^{2} + \sum_{i=1}^{8} U_{Bi}^{2}}$$

where:

$$U_A = \sqrt{\frac{\sum (y - y_{est})^2}{N - 2}}$$

where:

= measured sound pressure level of total noise (operating plus background) in dB y

= estimated sound pressure level of total noise from the regression analysis in dB Y<sub>est</sub>

Ν

= number of total noise measurement values in the wind speed bin corresponding to the integer wind speed.

All values for  $U_{A}$ ,  $U_{B9}$  and  $U_{C}$  are given in the annex.

#### 3.6.2 One-third octave band spectra

The uncertainty in the one-third octave band spectra is given in the Annex for all the third octave bands.

#### 3.6.3 Tonality

The uncertainty in the tonality is given in the Annex for all the given tones.

#### 4 Summary

As ordered by Siemens Wind Power A/S, 7330 Brande, Denmark, WINDTEST Kaiser-Wilhelm-Koog GmbH took measurements of the acoustic noise emissions on the Siemens WTGS 2.3 MW Mk II with a hub height of 80 m.



All measurements and analyses of the sound power level and tonality described in this report were made on the basis of the technical guideline [IEC 61400-11]. The analysis of the sound power level was carried out using the standardised wind speed which was calculated from the power curve provided by the customer (see Annex).

The data on the Siemens WTGS 2.3 MW Mk II have been evaluated by using a fourth order regression because this is the best fitting approximation over all relevant points.

The results of this measurement are given in table 4.

wind speed in 10 m height [m/s]	6	7	8	9	10
electrical power output calculated from the power curve [kW]	1049	1651	2106	2260	2295
measured pitch angle [degrees]	-0,8	-0,8	-0,8	0	>1
measured rotor speed [min <sup>-1</sup> ]	15,1	15,3	15,4	15,8	16,0
sound power level [dB]	103,4	104,9	105,1	105,0	105,0
combined uncertainty in the sound power level, U <sub>c</sub> [dB]	1,2	1,1	1,2	1,3	1,3
tonality, ∆L <sub>k</sub> [dB]	-5,58	-4,68	-6,36	-5,43	-5,91
tonal audibility, ∆L <sub>a,k</sub> [dB]	-2,58	-1,69	-3,36	-2,43	-3,58
frequency of the most prevalent tone [Hz]	1200	1200	1200	1200	530

 Table 4: Summary of results

It is assured that this report has been drawn up impartially in accordance with state-ofthe-art science and technology and with best knowledge and conscience.



5	List	of employed symbols and abbreviations	
d	-	distance from rotor centre to tower axis	m
D	-	rotor diameter	m
$\Delta L_{\text{tn,j,k}}$	-	tonality of the 'j th' spectrum at 'k th' wind speed, where $j = 1$ to 12 and $k = 6, 7, 8, 9, 10$	dB
$\Delta L_k$	-	energetic average of the 12 ∆L <sub>tn,j,k</sub>	dB
$\Delta L_{a,k}$	-	tonal audibility	dB
f	-	frequency of the tone	Hz
f <sub>c</sub>	-	centre frequency of critical band	Hz
Η	-	height of rotor centre (horizontal axis turbine) or height of rotor equatorial plane (vertical axis turbine) above local ground near the wind turbine	m
h₄	-	location point height (in measurement equal to microphone height)	m
κ	-	the ratio between standardised wind speed and measured wind speed	-
L <sub>A</sub> or L <sub>C</sub>	; -	A or C-weighted sound pressure level	dB
LAea.k	-	equivalent continuous A-weighted sound pressure level, where k =	
		6, 7, 8, 9, 10	dB
L <sub>Aeq,c,k</sub>	-	equivalent continuous A-weighted sound pressure level corrected for background noise at each integer wind speed and corrected to reference conditions, where $k = 6, 7, 8, 9, 10$	e dB
Ln	-	equivalent continuous sound pressure level level of the background	
1			aB
Lp I	-	sound pressure level of meaking noise within a critical hand in the "the"	ав
∟pn,j,k	-	spectrum at the 'k th' wind speed, where $j = 1$ to 12 and k = 6, 7, 8, 9, 10	) dB
L <sub>pn,avg,j,k</sub>	-	average of analysis bandwidth sound pressure levels of masking noise in the 'j th' spectrum at the 'k th' wind speed, where $j = 1$ to 12 and $k = 6, 7, 8, 9, 10$	dB
L <sub>pt,j,k</sub>	-	sound pressure level of the tone or tones in the 'j th' spectrum at the 'k th' wind speed, where $j = 1$ to 12 and $k = 6, 7, 8, 9, 10$	dB
Ls	-	equivalent continuous sound pressure level of only wind turbine noise	dB
L <sub>s+n</sub>	-	equivalent continuous sound pressure level of combined wind turbine and background noise	dB
L <sub>WA,k</sub>	-	apparent sound power level, where k = 6, 7, 8, 9, 10	dB
Ν	-	Number of measured values	-
Pw	-	effective electrical power	kW
R <sub>0</sub>	-	reference distance	m
Ri	-	slant distance from rotor centre to actual measurement position	m
S <sub>0</sub>	-	reference area, $S_0 = 1 m^2$	m
$U_{A},\ U_{B}$	-	Uncertainty components	dB
Uc	-	Total uncertainty	dB
U <sub>HG</sub>		Error in the background noise	dB
Vm	-	derived wind speed from power curve	m/s
Vs	-	standardised wind speed	m/s
WTGS	-	wind turbine generator system	-
У	-	measured sound pressure level of operating plus background noise	dB
<b>y</b> est	-	estimated sound pressure level of operating plus background noise from regression analysis	i the dB



#### 6 References

[IEC 61400-11] IEC 61400-11, Wind turbine generator systems - Part 11: Acoustic noise measurement techniques, Ed. 2.

#### 7 Annex

#### Annex 1: Measuring equipment used

Beschreibung description	Fabrikat supplier	Typ/type	WT Nr./Ser.Nr. WT stock number/serial number	Kal. am cal. on	Eichung am standardisatio n	Einsatz used
Akustischer Kalibrator acoustic calibrator	Bruel & Kjær	4231	WT 300083004 (2438819)	-	31.12.2006	x
Mikrofon	Bruel & Kjær	4188	zu WT 30002904 (2427565)	-	31.12.2006	x
Vorverstärker	Bruel & Kjær	ZC 0030	zu WT 30002904	- 31.12.2006		
Mikrofonkabel	Bruel & Kjær	AO 0560	zu WT 30002904	-	31.12.2006	x
Handschallpegelmesser	Bruel & Kjær	2238	WT 30002904 (2437622)	-	31.12.2006	x
Primärwindschirm	Brûel & Kjær	UA 0237	-	-	-	x
Sekundärwindschirm secondary wind shield	Delta Acoustics	SIM	-			
DAT-Rekorder	Sony	TCD-D100	WT 300083304 (541959)	-		×
Anemometer anemometer	Thies Clima	4.3519.00.000	WT 010041504 (PN 457 0604)	Jun. 04	-	x
Windrichtungsgeber wind direction sensor	Thies Clima	4.3129.00.012	WT 020013504 (0504426	-	-	x
Temperaturgeber temperature sensors	Heraeus (Logger)	PT100	WT 300084704	Jul. 05	•	x
Temperaturgeber temperature sensors	Heraeus (W+W)	PT100	WT 300084604	Jul. 05	-	x
Luftdruckgeber pressure sensors	Wilmers Messtechnik (Logger)	0619	WT 090021803	Jul. 05	-	x
Luftdruckgeber pressure sensors	Wilmers Messtechnik (W+W)	0619	WT 090022804	Jul. 05	-	x
Leistungsumformer power transducer	Metrawatt (DME 1)	SINEAX DME 442	WT 300070903	Jun. 04	-	
Leistungsumformer	Metrawatt (DME 2)	SINEAX DME 442	WT 300055202	Aug. 03	-	
Leistungsumformer power transducer	Metrawatt (DME 3)	SINEAX DME 442	WT 300018898	Feb. 05	-	
Leistungsumformer power transducer	Metrawatt (DME 4)	SINEAX DME 442	WT 300079804	Feb. 05	-	
Zangenstromwandler current clamps	Chauvin Arnoux (DME 1)	D32N	WT 300071603 bis 300071803	Jul. 05	-	
Zangenstromwandler current clamps	Chauvin Arnoux (DME 2)	D32N	WT 300053501 bis 300053701	Jul. 05	-	
Zangenstromwandler current clamps	Chauvin Arnoux (DME 3)	AmpFLEX A100	WT 300091804 bis 300092004	Jul. 05	-	
Zangenstromwandler current clamps	Chauvin Amoux (DME 4)	AmpFLEX A100	WT 300085804 bis 300086004	Jul. 05	-	
Datenlogger datalog	Th Friedrichs	1020	WT 030013504 (091630)	Jul. 04	-	x
Zweikanal-Echtzeit- Frequenzanalysator						
2-channel real time frequency	Brüel & Kjær	2144	WT 9904897 (1732981)	Sep. 03	-	x
Erfassungs- und Auswertesoftware	GfS Aachen	DiAdem 8.1				
data acquisition and analytical	DATALOG GmbH	Excel 2000 Dasy-Lab 7.0	-	-	-	x
Erfassungsrechner data acculsition Computer	HP	Compag nx 9005	WT 400023903 (CNF 3371X4F)		-	
Erfassungsrechner data acquisition Computer	HP	OmniBook XE3	WT 400021502 (TW 21806701)	-	-	
Errassungsrechner data acquisition Computer	HP	OmniBook XE3	WT 400020802 (TW 21121810) -		-	
data acquisition Computer	HP	Compaginx 5000	WT 400026604 (CNU43700RT)	-	-	
data acquisition Computer	HP	9005 2005	WT 400024003 (CNF 3371X70)	)0024003 (CNF 3371X70)		
data accuisition Computer 10 m - Teleskopmast	HP	9005	WT 400024103 (CNF 3371X4X)		-	×
10 m – telescopic most Unterbrechungsfreie	Clark (SMS 3)	QT 12MHP	WT 050019003	-	-	x
Spannungsversorgung uninterruptable power supply	APS	3mart 0P5 1000	WT 30009002104			x



#### Page 15 / 47







#### Page 16 / 47

#### Annex 2.1b: Higher order regression of $L_{Aeq}$ and $L_n$ against standardised wind speed





#### Page 17 / 47

#### Annex 2.2: Summary of analysis input parameters and results

Tated / P     =     2.30     MW       Tated / P     =     2.30     MW       NSg5% / WGg5% =     11.67     m/s       NSg5% / WGg5% =     11.67     m/s       berker [dB]     LAeq.c.k [dB]     LwA.k [dB]       37.9     55.4     103.4       37.9     55.4     103.4       40.2     57.0     104.9       41.9     57.1     105.0       42.6     57.1     105.0       43.5     57.1     105.0       isse L = f(WG)     LAeq.c.k [dB]     LwA.k [dB]       acker [dB]     LAeq.c.k [dB]     LwA.k [dB]       acker [dB]     LAeq.c.k [dB]     LwA.k [dB]       357.1     105.0     105.0       fisse L = f(WGsst)     57.1     105.0       Site / Standort     2300438	odus: Standard Mod leas. / Messdatum2005-08-1213 / Messung: IEC 61400-11 / Datenbasis: 1 Hz sampling / Bearbeiter: DiplIng. Joer	Ē																
nated / P_Nenn     =     2.3       nated / P_Nenn     =     2.3       NS95% / WG95% =     11.0       backgr [dB]     LAeq.c.k [dB]       37.9     55.4       37.9     55.4       40.2     57.0       42.6     57.0       44.9     57.1       isse L = f(WG)     1.Aeq.c.k [dB]       ackgr [dB]     LAeq.c.k [dB]       ackgr [dB]     Varadort       ackgr [dB]     WTGS-SNr.NreA.SNr.:	odus: Ieas. / Messdatum / Messung: 9 / Datenbasis: / Bearbeiter:	Høvsøre, De 2300439 Standard Mo				105.1	Lwa,k [dB]		105.0	105.0	105.1	104.9	103.4		Lwa,k [dB]		57 m/s	MW o
rated / P <sub>Nenn</sub> rated / P <sub>Nenn</sub> WS <sub>95%</sub> / WG 37.9 37.9 40.2 41.9 41.3 itse L = f(WG) itse L = f(WG) itse L = f(MG) solver [dB]	0 2 ~ m ~	dort: r./WEA-SNr.: dus:			(G <sub>5%</sub> )	57.1	LAeq.c.k [dB]		57.1	57.0	57.2	57.0	55.4		LAeq.c.k [dB]		<sub>95%</sub> = 11.	= 2.3
	Mode / M Date of r Standard Data basv In charge	Site / Stan WTGS-SN Mode / Mo			Ergebnisse L = f(W	43.5	Lbackgr [dB]	ebnisse L = f(WG)	47.3	44.9	42.6	40.2	37.9		Lbackgr [dB]		WS <sub>95%</sub> / WG	P <sub>rated</sub> / P <sub>Nenn</sub>
m L <sub>Aea</sub> k [dB] 55.5 57.1 57.3 57.3 57.3 57.3 57.3 57.3 57.3 57.3	:	_			VS <sub>95%</sub> ) / Tabelle 3: I	57.3	LAeq.k [dB]	VS) / Tabelle 2: Erg	57.5	57.3	57.3	57.1	55.5		L <sub>Aeq,k</sub> [dB]		ε	ε
A = 0.0 C = 112:0 WStom MStom MStom MStom WSt	Ergebnisse	3 MW Mk			ble 3: results L = f(V	8.38	WS <del>95%</del> WG95%	ble 2: results L = f(V	10	6	ω	7	Q	WG <sub>10m</sub>	WS <sub>10m</sub>		o = 112.0	A = 0.0
	Results / I	siemens 2.							[]		1		I		L		Ľ	£
3.50 m         3.50 m           3.50 m         0.050 m           1.12         1.12           1.3         1.3	I	U		1.3	1.3	1.2	1.1	1.2	Uc [dB]				ŝ				0.050 m	3.50 m
teparam m/s m/s = = = = = = = = = = = = = = = = = = =				5	4	8	5	4	[8]	\$	2		- 325.6	MM	s/m		"	H
Auswer d d d 2 2 2 3 8 3 9 1 40° 9 0 9 3 9 1 40° 9 0 9 0 9 0 9 0 0 0 0 0 0 0 0 0 0 0 0 0			herheiten	0.2	0.1	0.0	0.0	0.0	1 <sup>68</sup> U	<del>.</del>		0 03	284.40°	2.185	8.38		20 7	р
ation / ation	<i>]</i> ≇		Messunsic	68	64	4	31	44	[dB]	tät	sity / _	1	on / =	H	H			
O     m       0     m       0     m       0     m       355%(10m)     355%(10m)       355%(10m)     md direction       0     md direction       0     0       1     UAI       1     1	oog Gmb		Tabelle 1:	0.	0	o	ö	o	Ν	nzintensi	nce inten	ereicn	nd directi	ung <sub>95%</sub>	<sup>3</sup> 95%(10m)	ebnisse	Е 0	E
eters c = 80.( = 93. = 93. = 93. ts / Erg = 93. to / WC = 93. = 10 <sup>m</sup> / WC = 93. =	<b>TES!</b>		ncertainty /	0	6		7	9	10m	Turbuleı	s turbulei	asgnung	of the wir	<sub>5%</sub> / Leist	10m) / WG	s / Erg	- 93.	= 80.(
Param H = D = C D = Power <sub>9</sub> , WS 95% ( Power <sub>9</sub> , Windric K K Windric Windric K K the state of	0 5		ble 1: ur			-			SN ON	ttlere	erage		inge	wer	S <sub>95%</sub> (	esult	"	

WT 4498/05: Report of acoustical emissions of a Siemens wind turbine generator system of the type 2.3 MW Mk II near Høvsøre in Denmark



#### Annex 2.3: Plot of L<sub>WA</sub> against standardised wind speed





#### Annex 2.4: Plot of LAeq and Ln against measured wind speed



WT 4498/05: Report of acoustical emissions of a Siemens wind turbine generator system of the type 2.3 MW Mk II near Høvsøre in Denmark





Page 20 / 47



#### Annex 2.6: Plot of rotor speed against power




Page 22 / 47











Annex 3.1b: Overview spectra 7-12 of turbine noise at a wind speed of 6 m/s



### Page 25 / 47

### Annex 3.1c: Analysis of tonality of turbine noise at a wind speed of 6 m/s

charge / Bearbeiter: Dipl	Ē	)		,			
andard / Messung: IEC ind speed / Windge.: 6 m	Ches V	urbine noise 3etriebsaeräus:	of tonality of tu wertung des E	Analysis ( Tonhaltiqkeitsbe			WINDTEST
asurem. / Messdatum: 200	Me		21 13 Z. O 101 N		8		
e / Standort: Hav		MK II	MV 2 3 MV	Siemo			
tainty of delta La,k (Ua) =	Uncer						
<u>elta Lk - La (delta La,k) =</u>	<u>Audibility, d</u>						
<u>oility criterion (La) [dB] =</u>	<u>dependant audil</u>	Frequency					
<u>je of delta Lt (delta Lk) = </u>	Energetic avera						
-2.99	-2.73	36.74	34.02	18.82	2.00	1202	12
-2.99	-7.04	37.31	30.27	19.38	2.00	1202	5
-3.00	-5.22	36.85	31.62	18.92	2.00	1204	9
-2.99	-6.11	37.12	31.01	19.20	2.00	1202	o,
-2.99	-6.19	38.27	32.08	20.35	2.00	1202	ω
-3.00	-4.59	37.57	32.98	19.65	2.00	1204	2
-3.00	-8.83	38.90	30.07	20.97	2.00	1204	ω
-3.00	-7.73	37.49	29.77	19.57	2.00	1204	Q
-3.00	-7.26	38.12	30.86	20.19	2.00	1204	4
-3.00	-6.34	38.07	31.73	20.14	2.00	1204	m
-3.00	-4.42	38.33	33.91	20.40	2.00	1204	N
-3.00	-4.23	37.29	33.06	19.36	2.00	1204	-
[ab]	[dB]	[qb]	[qp]	[db]	[Hz]	[Hz]	
La de	delta Ltn.j.k	Lpn,J, k	Lpt.J.k	Lpn,avg,J,k	delta f	tone fT	Ο̈́Ν Έ
de l	٩	detta Ltn.j.k La	Lpn.j.k detta Ltn.j.k La	Lpt,j.k Lpn.j.k detta Ltn.j.k La	Lpn,avg.j.k Lpn,j.k detta Ltn.j.k La	delta f Lpn,avgj.k Lpt.j.k Lpn.j.k delta Ltn.j.k La	tone fT detta f Lpn,avg.j,k Lpt,j,k Lpn,j,k detta Ltn.j,k La













### Annex 3.2c: Analysis of tonality of turbine noise at a wind speed of 7 m/s

Page 28 / 47

	DiplIng. Ulf Kock	charge / Bearbeiter	ln c		0	0		g GmbH	itser-withetim-Koo	ž
	7 m/s	nd speed / Windge.	New Mark	etriebsneräusch	vertung des Bi	Tonhaltickeitsbev		)) :		5 :
	IEC 61400-11/Ed 2	indard / Messung:	5	rbine noise	of tonality of tu	Analvsis c				
	2005-08-12/13	asurem. / Messdatum:	Me							
	Høvsøre	e / Standort:	Site	V Mk II	ens 2.3 MV	Sieme				-
	-3.0 dB ?: Yes	ter than or equal to .	<u>Audibility grea</u>				-			
1 source 1	<u> Ua) = 2.43 [dB]</u>	tainty of deita La.k (I	Uncer							
Lno'T :sli	<u>,k) = -1.69 [dB]</u>	eita <u>Lk - La (deita La</u>	<u>Audibility, de</u>							
SM_IEC	B] = -3.00 [dB]	<u>vility criterion (La) [d</u>	<u>ependant audit</u>	Frequency de						
L	<u>-k) = -4.68 [dB]</u>	<u>ie of deita Lt (deita L</u>	nergetic averac	Ш						
	0.36	-2.99	-2.64	38.82	36.18	20.90	2.00	1202	12	
	-0.68	-2.99	-3.68	40.29	36.62	22.37	2.00	1202	1	
	-1.83	-3.00	-4.83	40.41	35.58	22.48	2.00	1204	9	-
	-5.75	-3.00	-8.75	40.27	31.52	22.34	2.00	1204	5	
	-5.60	-3.00	-8.60	40.00	31.40	22.07	2.00	1204	¢	
	-5.87	-3.00	-8.87	39.55	30.69	21.62	2.00	1204	~	
	-2.78	-2.99	-5.78	39.80	34.03	21.88	2.00	1202	9	
lenð	0.18	-2.99	-2.82	39.78	36.97	21.86	2.00	1202	Q	
a alitofic	-0.26	-3.00	-3.26	39.06	35.80	21.13	2.00	1204	4	
bay_vepy)	-0.60	-2.99	-3.59	39.36	35.77	21.44	2.00	1202	m	
-MG	-2.57	-3.00	-5.57	38.95	33.39	21.03	2:00	1204	2	
	-0.94	-3.00	-3.93	38.65	34.72	20.72	2.00	1204	-	
	[dB]	[qb]	[dB]	[dB]	[dB]	[dB]	[Hz]	[Hz]		
60 40	delta La, k	۲ ۲	delta Ltn.j, k	Lpn.J, k	Lpt.J.k	Lpn,avg,j,k	delta f	tone fT	Ш No	
\$00										





Annex 3.3a: Overview spectra 1-6 of turbine noise at a wind speed of 8 m/s







Г

	DiplIng. UIF Kock	charge / Bearbeiter	Ē		5 m B		-	Hqm	ar-Wihelm-Koog (
	IEC 61400-11/Ed.2 8 m/s	andard / Messung: ind speed / Windge.	25 ×	rbine noise etriebsneräusch	or tonality or tu wertung des Bi	Analysis ( Tonhaltickeitsbev			INDTEST
	2005-08-12/13	asurem. / Messdatum.	Me	•		•	7		
	Høvsøre	e / Standort:	St	V Mk II	ens 2.3 MV	Sieme			
	-3.0 dB ?: No	ater than or equal to	Audibility gre						
	<u> Ua) = 2.56 [dB]</u>	<u>tainty of delta La,k (</u>	Uncer						
NOT IN	<u>,k) = -3.36 [dB]</u>	<u>elta Lk - La (delta La</u>	<u>Audibility, d</u>						
021 113	<u> B] = -2.99 [dB]</u>	<u>bility criterion (La) [d</u>	<u>ependant audil</u>	Frequency d					
0	K) = -0.30 (DB)	de ol deita Lt (deita L	neigeuc avera	ני					
	-5.13	-3.00	-8.13	39.59	31.46	21.66	2.00	1204	12
	-5.41	-2.99	-8.41	40.36	31.96	22.44	2.00	1202	1
	-5.67	-2.99	-8.67	39.70	31.03	21.77	2.00	1202	0
	-6.08	-3.00	80.6-	39.37	30.29	21.44	2.00	1204	σ
	-2.96	-2.99	-5.95	38.48	32.53	20.56	2.00	1202	œ
	-8,55	-2.99	-11.54	40.05	28.51	22.13	2.00	1202	2
	-4.75	-2.99	-7.74	43.21	35.47	25.29	2.00	1202	9
	-5.79	-2.99	-8.78	43.70	34.91	25.78	2.00	1202	S
	-3.25	-2.99	-6.25	42.95	36.71	25.03	2.00	1202	4
	-1.25	-2.99	-4.24	41.02	36.78	23.10	2.00	1202	ю
	0.03	-2.99	-2.97	39.88	36.91	21.96	2.00	1202	2
	-0.25	-2.99	-3.24	42.09	38.84	24.17	2.00	1202	-
	[dB]	[dB]	[dB]	[dB]	[dB]	[dB]	[Hz]	[Hz]	
	detta La, k	e	delta Ltn.j,k	Lpn,j, k	Lpt.J.k	Lpn,avg.j,k	delta f	tone fT	No











### Annex 3.4c: Analysis of tonality of turbine noise at a wind speed of 9 m/s

Page 34 / 47

	9 m/s DiplIng. Ulf Kock	nd speed / Windge. sharge / Bearbeiter:	hes w	etriebsgeräusc	vertung des B	<b>Fonhaltigkeitsbe</b>	 I	g GmbH	er-Wilhelm-Koog
	IEC 61400-11/Ed 2	Indard / Messung:	Sta	rbine noise	of tonality of tu	Analysis o			NDTEST
	2005-08-12/13	asurem. / Messdatum;	Me				2		
	Høvsøre	e / Standort:	Site	V Mk II	ens 2 3 MV	Sieme			
	-3.0 dB ?: Yes	ter than or equal to	<u>Audibility grea</u>						
t eonuoS	<u> Ua) = 2.32 [dB]</u>	tainty of delta La,k (I	Uncert						
_noT ;ski	<u>,k) = -2.43 [dB]</u>	<u>elta Lk - La (delta La</u>	<u>Audibility, de</u>						
OBI MS	<u> B] = -2.99 [dB]</u>	<u>ility criterion (La) Id</u>	<u>lependant audit</u>	Frequency o					
6	<u>_k) = -6.43 [dB]</u>	<u>ie of delta Lt (delta L</u>	chergetic averag	Шî					
	-2.86	-2.99	-5.85	44.01	38.16	26.09	2.00	1202	12
	-1.54	-2.99	-4.54	43.20	38.67	25.28	2.00	1202	<b>F</b>
	-2.60	-2.99	-5.59	42.42	36.83	24.50	2.00	1202	9
	-5.64	-2.99	-8.63	40.12	31.49	22.20	2.00	1202	თ
	-4.37	-2.99	-7.37	39.45	32.08	21.53	2.00	1202	ω
	-2.77	-2.99	-5.76	40.52	34.75	22.59	2.00	1202	2
	-1.28	-2.99	-4.28	39.36	35.08	21.44	2.00	1202	9
le 10	-2.14	-2.99	-5.13	39.48	34.35	21.56	2.00	1202	5
a alti chic	-2.48	-3.00	-5.48	39.46	33.98	21.53	2.00	1204	4
paj_/aib_/	-1.94	-2.99	-4.93	39.28	34.35	21.36	2.00	1202	e
9MJ	-1.29	-2.99	-4.28	40.51	36.23	22.59	2.00	1202	N
	-2.09	-2.99	-5.09	39.13	34.04	21.21	2.00	1202	-
	[dB]	[dB]	[dB]	[dB]	[dB]	[dB]	[Hz]	[Hz]	
60 40	detta La, k	Ľ	delta Ltn.j, k	Lpn,J, k	Lpt.J.k	Lpn,avg.j,k	delta f	tone fT	о́ N





Annex 3.5a: Overview spectra 1-6 of turbine noise at a wind speed of 10 m/s









### Annex 3.5c: Analysis of tonality of turbine noise at a wind speed of 10 m/s

Page 37 / 47

	Dipl -Ing Ulf Kock	charge / Bearbeiter	ln e						<b>A</b>
	10 m/s	ind speed / Windge.	hes	etriebsgeräusc	vertung des B	Tonhaltigkeitsbev	-		<b>vii vii heim-Kood Gmi</b>
	IEC 61400-11/Ed.2	indard / Messung:	<i>t</i> 5	Irbine noise	of tonality of tu	Analysis c			VINDTECT
	2005-08-12/13	asurem. / Messdatum:	Me				a		
	Høvsøre	e / Standort:	Sit	V Mk II	ens 2.3 MV	Sieme			
oş	0-3.0 dB ?: No	ater than or equal to	Audibility gre						
, siyeon	<u> Ua) = 3.13 [dB]</u>	tainty of deita La,k (	<u>Uncer</u>						
.M8_noT	.k) = -3.58 [dB]	<u>elta Lk - La (delta La</u>	<u>Audibility, de</u>						
ÌEC 233	<u> 18] = -2.33 [dB]</u>	<u>oility criterion (La) I</u> d	lependant audit	Frequency d					
01 <sup>~~</sup> ZH	<u>_k) = -5.91 [dB]</u>	<u>ie of delta Lt (delta L</u>	<u>inergetic averac</u>	ш					
	1.90	-2.34	80. <sup>0</sup> -	\$0.0 <del>4</del>	- 0.04	5	2	5	!
							000	E2.4	¢,
	-0.03	-2.33	-2.36	47.03	44.67	31.04	2.00	526	1
	-2.53	-2.33	-4.87	47.03	42.17	31.04	2.00	530	9
	-4.87	-2.33	-7.20	47.52	40.32	31.53	2.00	528	თ
	-5.29	-2.33	-7.62	47.00	39.38	31.00	2.00	530	Ð
	-0.85	-2.34	-3.19	47.08	43.89	31.08	2.00	534	7
	-13.65	-2.32	-15.98	47.23		31.25	2.00	524	Q
භව	-13.67	-2.34	-16.00	47.99		31.98	2.00	534	Q
a ahichiq	-3.12	-2.33	-5.44	46.79	41.35	30.81	2.00	526	4
) "Q(9/ "ך 60	-13.68	-2.34	-16.02	47.77		31.75	2.00	540	m
гме	-13.65	-2.32	-15.97	47.69		31.72	2.00	520	N
	-13.67	-2.34	-16.01	47.81		31.80	2.00	536	~
	[dB]	[dB]	[qB]	[dB]	[dB]	[dB]	[Hz]	[Hz]	
60 20	delta La, k	-					חפווק ו	tone ti	ĎE =



### Annex 4.1: A-weighted sound pressure 1/3-octave spectrum at 6 m/s

Page 38 / 47





Page 39 / 47









### Annex 4.4: A-weighted sound pressure 1/3-octave spectrum at 9 m/s

Page 41 / 47







Annex 4.5: A-weighted sound pressure 1/3-octave spectrum at 10 m/s







Picture from the board in direction of the WTGS





Picture of microphone and board



# Bonus 2.3 MW Mk II, 1.225 kg/m3 Sales Power Curve, Preliminary

The calculated power curve data are valid for the above air density conditions, clean rotor blades, and horizontal, undisturbed air flow with 10% turbulence intensity.



The annual energy production data for different annual mean wind speeds in hub height are calculated from the above power curve assuming a Rayleigh wind speed distribution, 100 percent availability, and no reductions due to array losses, grid losses, or other external factors affecting the production.



HST

Bonus Enerav A/S

1/1



#### Herstellerbescheinigung zu spezifischen Daten der Anlage vom Typ Manufacturer's certificate on specific data of the type of installation

Datum / date: 22/08/2005

1. Allgemeines		Gener
Hersteller	Siemens Wind Power A/S	manufacturer
Anlagenbezeichnung	2.3 MW mkli	type name
Art (horizontale/vertikale Achse)	Horizontal	type (horizontal / vertical axls)
Nennleistung	2300 kW	rated power
Nabenhöhe über Grund	80 m	hub height above ground
Nabenhöhe über Fundamentflansch	80 m	hub height above top of foundation flang
Nennwindgeschwindigkeit	12 m/s	rated wind speed
Ein- und Ausschaltwindgeschwindigkeit	3/25 m/s	cut-in and cut-out wind speed
Beitrag zum Kurzschlussstrom	appr. 2.5 kA	contribution to short circuit current
2. Rotor	l	Roto
Durchmesser	92.4 m	diameter
Bestrichene Fläche	6706 m²	swept area
Anzahl der Blätter	3	number of blades
Nabenart (pendeInd/starr)	Rigid	kind of hub (teetered/rigid)
Anordnung zum Turm (luv/lee)	Luv	relative position to tower (luv/lee)
Nenndrehzahl / -bereich	6,1-18,4 U/min / rpm	rated speed / speed range
Auslegungsschnellaufzahl		design tip speed ratio
Rotorblatteinstellwinkel	-2 to 82° Pitch controlled	rotor blade pitch setting
Konuswinkel	2°	cone angle
Achsneigung	6°	tilt angle
Abstand Rotorflanschmittelpunkt -		distance between rotor flange centre and
Turmmittellinie	3.5 m	tower centre line
. Blatt	I	Biade
Hersteller	Siemens Wind Power A/S	manufacturer
Typenbezeichnung	B45	type
Profile innen/außen	FFAW3/ NACA63-6xx	blade section inner/outer
Material	GRE	material
Länge	45 m	length
Profiltiefe max./min.	3.35 m/ 0.7 m	chord length (max./min.)
Zusatzkomponenten (z.B. stall strips,	Vortex generator	additional components (e.g. stall strips
Vortex-Generatoren, Turbulatoren)	-	vortex generators, trip strips)
Extenderlänge	N/A	extender length
. Getriebe		Gear
Hersteller	Flender	manufacturer
Typenbezeichnung	PEAB 4456	type
Ausführung	Planetary/helical	design
Übersetzungsverhältnis	1 90.84	speed ratio
Generator		Generator
Hersteller		Cenerator
Typenbezeichnung	AN645001 44	time
Anzahl	1	
Art	Asynchronous	design
Nennleistung(en)		design
Nennelatung(en)		rated power (s)
Nennscheimeistung	2090 KVA	rated apparent power
	750 V @1550	rated speed (s)/ speed range
Spannung	750 V @ 1550rpm	voltage
Nennechlunf		nequency
Nemachupi	70	rated slip
Turm		
Hersteller		manufacturar
Turm Hersteller Typenbezeichnung		manufacturer
Hersteller Typenbezeichnung Ausführung (Gitter/Pohr, mit (kon.)	DSSM04	manufacturer type
. Turm Hersteller Typenbezeichnung Ausführung (Gitter/Rohr, zyl./kon.)	DSSM04 Tapered turbular	manufacturer type design (lattice/tubular, cylindrical/ conical)

Seite 1 von 2

### Annex 7b: Manufacturer's certificate, page 2



7. Windrichtungsnachführung		Yaw control
Ausführung (aktiv/Passiv)	Active	design (active/passive)
Antriebsart (el./mech./hydr.)	Electrical	drive (electr./mech./hvdr.)
Dämpfungssystem während des Betriebes	Friction	damping system during operation
8. Betriebsführung/ Regelung		Other electric installations
Art der Leistungsregelung	Pitch control	kind of power control
Antrieb der Leistungsregelung	Blade pitch	actuation of power control
Hersteller der Betriebsführung/ Regelung	KK-electronic	manufacturer of control system
- Typenbezeichnung	WTC 3	- type
- Verwendete Steuerungskurve		- applied used control characteristics
9. Sonstige elektrische Komponenten		Other electric installations
Anzahl der Kompensationsstufen	Controlled by use of	number of compensation stages
	4 quadrant	
	frequency converter	
Blindleistung Stufe 1	kvar	reactive power stage 1
Art der Netzkopplung	Connected by use	kind of interconnection
	of frequency conv.	
- Hersteller	Alstom	- manufacturer
- Typenbezeichnung	4 quadrant	- type
-	frequency conv.	-
Netzschutzhersteller	KK	mains protective manufacturer
- Typenbezeichnung		- type
- Einstellbereiche:		- adjustment ranges:
Spannungssteigerungsschutz	759 V line-line	overvoltage protection
Spannungsrückgangsschutz	621 V line-line for	undervoltage protection
	more than 3 sec.	
Frequenzsteigerungsschutz	51,5 Hz	overfrequency protection
Frequenzrückgangsschutz	47,5 Hz	underfrequency protection
Typenbezeichnung der Abschalteinheit	Short circuit breaker	type of contact break device
Oberschwingungsfilter (Ja/Nein)	Yes	harmonic filter (yes/no)
(Oberschwingungsfilter müssen auf den		(harmonic filter have to be designed for the
Netzverknüfpungspunkt ausgelegt sein.)		point of common coupling)
10. Bremssystem		Brake system
Bremssystem (primär/sekundär)	Blade / Mech. brake	brake system (primary/secondary)
- Aktivierung	Hydraulic	- activation
- Anordnung	Hydraulic	- location
- Bremsenart	Pitch blade/ brake disc	– type
- Betätigung	Active / Passive	- actuation
11. Typenprüfung		Type test
Prüfbehörde	DNV	testing authority
Aktenzeichen		reference
12. Informativer Tell	I	Informative
Standort der vermessenen WEA	Høvsøre DK	location of measured WTGS
Koordinaten des Standorts		coordinate of location
Seriennummer der WEA	2300439	Serial number of WTGS
der Blätter	1001/ 1002/ 1003	blades
des Getriebes	4803384 020 1 200 100 100 100	gearbox
des Generators	457691 🍮 🛛 🗲 🛛 🗸 🕻	generator
Anschrift des Herstellers	Siemens Wind Pow Positiox 171 - Boru DK-7330 Brande - I	er AIS ovej 16 Denmark
Address of manufacturer	lei. +45 9942 2222	Stempel, Unterschrift stamp, signature
		stamp; signature

Der Hersteller der Windenergieanlage bestätigt, daß die WEA, deren Schallemission, Leistungskurve und elektrischen Eigenschaften in den Prüfberichten abgebildet ist, hinsichtlich ihrer technischen Daten mit den o.g. Positionen identisch ist.

The manfacturer of the wind turbine generator system confirms that the WTGS whose noise level, power curve and grid compatability is measured and depicted in the test report xxxxxxx is identical with the above entries with regard to its technical data.

Seite 2 von 2

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#### www.siemens.com/energy

The new standard for moderate wind conditions

Siemens Wind Turbine SWT-2.3-101

Answers for energy.



## **SIEMENS**

# Your trusted partner

Siemens has been a major driver of innovation in the wind power industry since the early 1980s when wind turbine technology was still in its infancy.

Technology has changed with the times, but Siemens' commitment to providing its customers with proven wind turbine solutions remains the same.

The combination of robust and reliable turbines, highly efficient solutions for power transmission and distribution and a deep understanding of the entire energy market ensures that Siemens will continue to be a leading supplier.

Siemens' record, when it comes to on-time delivery, is impeccable. Long-lasting customer relationships, based on the successful installation of wind turbines, provide for a sound, sustainable and profitable investment.

Drawing on 140 years of experience in the energy sector, a strong focus on renewables and a global network of highly skilled and trained employees, Siemens has proven itself to be a trustworthy and reliable business partner. And will continue to be in the future.

# Harvest more energy from sites with moderate wind conditions

The Siemens SWT-2.3-101 turbine is designed to deliver unparalleled performance and reliability, making it especially suited to areas with moderate wind conditions.

> The SWT-2.3-101 turbine offers low energy production costs, and joins Siemens' 2.3-MW product family, which has proven availabilitity that is among the highest in the industry. The 101-meter rotor is specifically designed to optimize the energy output in areas with moderate wind conditions. The turbine is also ideal for all types of grid connections in most major markets.

The SWT-2.3-101 is designed to last. The robust and reliable design offers a high yield with low maintenance costs. The turbine is backed by advanced condition monitoring and diagnostics, which constantly examine







the turbine. Any change in a turbine's performance is promptly addressed by an experienced after-sales service team either remotely or in the field.

If you desire a better return on investment and superior availability, take a closer look at the SWT-2.3-101 turbine.

3

# Superior performance gives higher yields

#### Optimum energy at moderate wind conditions

#### Harvesting more energy

The SWT-2.3-101 wind turbine is designed to increase the energy returns from sites with moderate wind conditions. Advanced blade technology also allows for guieter operation. The B49 blade with a rotor diameter of 101 meters and pitch regulation optimizes power output and increases control over the energy output.

#### **High availability**

Currently, the Siemens fleet of 2.3-MW wind turbines sets the industry standard for availability. The SWT-2.3-101 will build on the reputation for reliability that the market has come to expect from a Siemens Wind turbine.

#### High yield with minimal maintenance

Siemens optimizes the return on investment in its wind turbines through intelligent maintenance that ensures the turbine to deliver high yield with low operational costs.

The rugged structural design, combined with an automatic lubrication system, internal climate control and a generator system

without slip rings contributes to exceptional reliability. The innovative design of the SWT-2.3-101 allows for longer service intervals.

#### Superior grid compliance

The Siemens NetConverter<sup>®</sup> system is designed for maximum flexibility in the turbine's response to voltage and frequency variations, fault ride-through capability and output adjustment. The advanced wind farm control system provides state-of-the-art fleet management.

#### Proven track record

Siemens has a proven track record of providing reliable turbines that last. The world's first offshore wind farm in Vindeby, Denmark, was installed in 1991 and is still fully operational. In California, Siemens installed over 1,100 turbines between 1983 and 1990, with 97% still in operation today. Siemens takes its commitment to reliability seriously and prides itself on the long lifespan that its turbines have demonstrated.



## No compromise on reliability

#### Designed for life

Siemens turbines are designed to last. The robust design of the SWT-2.3-101 allows for trouble-free output throughout the complete lifecycle of the turbine.

The blades are made of fiberglass-reinforced epoxy in Siemens' proprietary IntegralBlade<sup>®</sup> manufacturing process. The blades are cast in one piece in a closed process, which eliminates the traditional weaknesses found at glue joints in other manufacturers' blades. Like the turbine itself, the blades are designed to last.

Climate control within the turbine protects vital equipment from the outside environment. The turbine also offers controlled-wear strategies for critical components, which results in a further reduction of maintenance costs.

#### Safety first

Safety is at the heart of all Siemens operations. From production to installation, operation and service, Siemens strives to set the standard in safety.

The fail-to-safe capabilities within a turbine, combined with Siemens' superior lightning protection system, are designed to enhance security for the turbine.

#### Advanced operations support

Given the logistical challenges associated with servicing wind farms, Siemens has equipped its turbines with a Turbine Condition Monitoring (TCM) system that reduces the need for on-site servicing.

Continuous monitoring of turbines allows for the discovery of small faults before they become major problems.

The TCM system continuously checks the external and internal condition of the wind turbine. Twenty-four hours a day, seven days a week precise measurements are taken of vibrations in the gearbox, the generator and the main shaft bearings. The system instantly detects deviations from normal operating conditions.

Using the knowledge gained from monitoring thousands of turbines over the years, Siemens' experts are exceptionally skilled at analyzing and predicting faults within a turbine. This allows Siemens to proactively plan the service and maintenance of the turbines as each fault can be categorized and prioritized based on the severity of the fault. Siemens can then determine the most appropriate course of action to keep the turbine running at its best.

# **Technical specifications**



	6
2	3

Rotor	
Diameter Swept area Rotor speed Power regulation	101 m 8,000 m <sup>2</sup> 6-16 rpm Pitch regulation with variable speed
Blades	
Type Length	B49 49 m
Aerodynamic brake	
Type Activation	Full-span pitching Active, hydraulic
Transmission system	
Gearbox type Gearbox ratio Gearbox oil filtering Gearbox cooling Oil volume	3-stage planetary/helical 1:91 Inline and offline Separate oil cooler Approximately 400 l
Mechanical brake	
Туре	Hydraulic disc brake

#### Generator Asynchronous Туре Nominal power 2,300 kW Voltage 690 V Cooling system Integrated heat exchanger Yaw system Туре Active Monitoring system SCADA system WebWPS Remote control Full turbine control Tower Туре Cylindrical and/or tapered tubular Hub height 80 m or site-specific **Operational data** Cut-in wind speed 3-4 m/s 12-13 m/s Rated power at Cut-out wind speed 25 m/s Maximum 3 s gust 55 m/s (standard version) 60 m/s (IEC version) Weights Rotor 62 tons Nacelle 82 tons Tower for 80-m hub height 162 tons

#### Sales power curve

The calculated power curve data are valid for standard conditions of 15 degrees Celsius air temperature, 1013 hPa air pressure and 1.225 kg/m<sup>3</sup> air density, clean rotor blades and horizontal, undisturbed air flow. The calculated curve data are preliminary.



6



#### Nacelle arrangement

- 1. Spinner
- 2. Spinner bracket
- 3. Blade
- 4. Pitch bearing
- 5. Rotor hub
- 6. Main bearing
- 7. Main shaft
- 8. Gearbox
- 9. Brake disc

- 10. Coupling
- 11. Generator
- 12. Service crane
- 13. Meteorological sensors
- 14. Tower
- 15. Yaw ring
- 16. Yaw gear
- 17. Nacelle bedplate
- 18. Oil filter
- 19. Canopy
- 20. Generator fan



## SWT-2.221-101 Low Noise, Hub Height 99.5 m **Acoustic Emission**

#### **Sound Power Levels**

The warranted sound power levels are presented with reference to the code IEC 61400-11:2002 with amendment 1 dated 2006-05 based on a hub height of 99.5 m and a roughness length of 1.661 m as described in the IEC code. The sound power levels (Lwa) presented are valid for the corresponding wind speeds referenced to a height of 10 m above ground level.

Wind speed [m/s]	4	5	6	7	8	9	10	11	12	Up to cut-out
Sound Power Level	105.0	105.0	105.0	105.0	105.0	105.0	105.0	105.0	105.0	105.0

Table 1: Noise emission, Lwa [dB(A) re 1 pW]

#### **Typical Octave Band**

Typical, not warranted octave band spectra are tabulated below for 6 and 8 m/s referenced to 10 m height.

Octave band, centre frequency [Hz]	63	125	250	500	1000	2000	4000	8000
Sound Power Level	82.6	93.8	97.0	99.5	99.6	97.1	89.3	84.9
Table 2: Typical octave band for 6 m/s								

Octave band, centre frequency [Hz]	63	125	250	500	1000	2000	4000	8000
Sound Power Level	82.4	93.0	96.0	99.8	100.1	96.5	89.6	85.7
Table 3: Typical octave hand for 8 m/s								

Table 3: Typical octave band for 8 m/s



## SWT-2.126-101 Low Noise, Hub Height 99.5 m **Acoustic Emission**

#### **Sound Power Levels**

The warranted sound power levels are presented with reference to the code IEC 61400-11:2002 with amendment 1 dated 2006-05 based on a hub height of 99.5 m and a roughness length of 1.800 m as described in the IEC code. The sound power levels (Lwa) presented are valid for the corresponding wind speeds referenced to a height of 10 m above ground level.

Wind speed [m/s]	4	5	6	7	8	9	10	11	12	Up to cut-out
Sound Power Level	104.0	104.0	104.0	104.0	104.0	104.0	104.0	104.0	104.0	104.0

Table 1: Noise emission, Lwa [dB(A) re 1 pW]

#### **Typical Octave Band**

Typical, not warranted octave band spectra are tabulated below for 6 and 8 m/s referenced to 10 m height.

Octave band, centre frequency [Hz]	63	125	250	500	1000	2000	4000	8000
Sound Power Level	83.1	94.1	96.6	97.8	97.9	96.5	88.4	84.0
Table 2: Typical octave band for 6 m/s								

Octave band, centre frequency [Hz]	63	125	250	500	1000	2000	4000	8000
Sound Power Level	82.2	92.5	94.8	98.5	99.1	95.5	89.0	85.1
Table 3: Typical octave hand for 8 m/s								

Table 3: Typical octave band for 8 m/s



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					E		
					_		
					D		
					4-		
					с		
		1					
SWI-2.3	-101	400 500	140 500	150.000	-		
Lub hoight		130.500m	140.500m	150.000m	-		
Hub neight		80.000m	90.000m	99.500m			
Tower height		78.540m	88.540m	98.040m			
Tower to		2392mm	239211111 4200mm	2060mm	-		
Tower bo	diom diameter	420011111	420011111	390011111	-		
	Motri				4		
	Matr.:		Toon format:	1			
Opstalt S Elevation S	WT-2.3-101 SWT-2.3-101		Draw. format:				
eller gøres tilgængeligt tilladelse. ftalt med os. retsforfølgelse. ens Wind Power A/S d or made available to a		IENS	Tegn. skala/D	braw. scale:	A		
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	-						

### Stantec GRAND RENEWABLE ENERGY PARK WIND TURBINE SPECIFICATIONS REPORT

# **Attachment B**

**Turbine Locations**
Turbine ID	<b>UTM_X</b>	UTM_Y	DATUM
1	607287	4746785	NAD83, UTM Zone 17
2	605035	4746639	NAD83, UTM Zone 17
3	606942	4746830	NAD83, UTM Zone 17
4	604861	4746993	NAD83, UTM Zone 17
5	602757	4745791	NAD83, UTM Zone 17
6	606513	4747319	NAD83, UTM Zone 17
7	608495	4747949	NAD83, UTM Zone 17
8	607477	4747512	NAD83, UTM Zone 17
9	600290	4745005	NAD83, UTM Zone 17
10	593994	4748442	NAD83, UTM Zone 17
11	603472	4748075	NAD83, UTM Zone 17
12	601479	4747111	NAD83, UTM Zone 17
13	594663	4751618	NAD83, UTM Zone 17
14	603952	4750047	NAD83, UTM Zone 17
15	608232	4749798	NAD83, UTM Zone 17
16	594352	4749960	NAD83, UTM Zone 17
17	598648	4747922	NAD83, UTM Zone 17
18	587941	4753452	NAD83, UTM Zone 17
19	606366	4749368	NAD83, UTM Zone 17
20	592573	4749463	NAD83, UTM Zone 17
21	602692	4746290	NAD83, UTM Zone 17
22	601756	4751401	NAD83, UTM Zone 17
23	591178	4751634	NAD83, UTM Zone 17
24	592280	4749799	NAD83, UTM Zone 17
25	599133	4750265	NAD83, UTM Zone 17
26	607589	4749481	NAD83, UTM Zone 17
27	598999	4748313	NAD83, UTM Zone 17
28	591339	4/522/3	NAD83, UTM Zone 17
29	599967	4750467	NAD83, UTM Zone 17
30	000959	4749603	NAD83, UTM Zone 17
33	589588	4755581	NAD83, UTM Zone 17
34 25	589/90	4753921	NAD83, UTM Zone 17
35	500002	4749032	NADOS, UTM ZONE 17
27	602481	4733707	NAD83, UTM Zone 17
38	602608	4749039	NAD83, UTM Zone 17
39	603875	4749409	NAD83, UTM Zone 17
40	604239	4749614	NAD83_UTM Zone 17
41	590395	4753879	NAD83, UTM Zone 17
42	600381	4750377	NAD83, UTM Zone 17
43	588466	4752970	NAD83, UTM Zone 17
44	599489	4748483	NAD83, UTM Zone 17
45	590085	4753880	NAD83, UTM Zone 17
46	590582	4751836	NAD83, UTM Zone 17
47	604740	4750499	NAD83, UTM Zone 17
48	594126	4750504	NAD83, UTM Zone 17

49	608750	4749784	NAD83, UTM Zone 17
50	609091	4749844	NAD83, UTM Zone 17
51	601762	4745085	NAD83, UTM Zone 17
52	599708	4748016	NAD83, UTM Zone 17
53	600301	4748359	NAD83, UTM Zone 17
54	607370	4746400	NAD83, UTM Zone 17
55	600136	4746677	NAD83, UTM Zone 17
56	598675	4750335	NAD83, UTM Zone 17
57	606650	4751283	NAD83, UTM Zone 17
58	589733	4750362	NAD83, UTM Zone 17
59	614355	4748118	NAD83, UTM Zone 17
60	614974	4747470	NAD83, UTM Zone 17
61	614326	4747732	NAD83, UTM Zone 17
62	614680	4748176	NAD83, UTM Zone 17
63	614750	4747811	NAD83, UTM Zone 17
64	614705	4747338	NAD83, UTM Zone 17
65	611480	4747403	NAD83, UTM Zone 17
66	611758	4747387	NAD83, UTM Zone 17
67	612236	4747633	NAD83, UTM Zone 17
68	602131	4748909	NAD83, UTM Zone 17
69	606923	4747368	NAD83, UTM Zone 17



Notes

- Samsung GREP Turbine
- Other Proponent Turbine
- Road
- Property Boundary
- Conservation Area
- Provincial Park
- Waterbody
- **Noise Receptor** Participant
  - Receptor
  - Vacant Lot Surrogate Receptor

## **Stantec**

Coordinate System: UTM NAD 83 - Zone 17.
Data Sources: Ontario Ministry of Natural Resources © Queens Printer Ontario, 2009; © Samsung, 2010; © NextEra, 2010; © Zephyr North, 2010.

June 2011 160960577

Client/Project

Figure No.

Title

DRAFT

MAP

SAMSUNG, PATTERN & KEPCO (SPK) GRAND RENEWABLE ENERGY PARK

PRELIMINARY LAYOUT